SDMS DocID

455166

Superfund Records Center

SITE: Wells GRH

BREAK: 23 OTHER: 455166

## FRE COM DO NY MARK

#### ADDENDUM I TO HYDROGEOLOGIC CHARACTERIZATION REPORT (Volume 1 of 2)

MURPHY'S WASTE OIL SERVICE, INC. 252 SALEM STREET WOBURN, MASSACHUSETTS

January 31, 1995

Prepared for:

Murphy's Waste Oil Service, Inc. 252 Salem Street Woburn, MA 01801

Prepared by:

Clean Harbors Environmental Services, Inc. 325 Wood Road Braintree, MA 02184

CHES Job No. EN-170



1200 CROWN COLONY DRIVE, P.O. BOX 9137 • QUINCY, MA 02269-9137 (617) 849-1800

WRITER'S DIRECT NUMBER

Extension 4182

LAW DEPARTMENT (617) 849-1800 FAX (617) 786-9716

January 31, 1995

Mr. John A. Carrigan
Department of Environmental Protection
Hazardous Waste Regulatory Program
1 Winter Street
Boston, Massachusetts 02108

Re: Murphy's Waste Oil Service, Inc.
Addendum I to Hydrogeologic
Characterization Report

Dear Mr. Carrigan:

Enclosed please find two (2) copies of a document entitled "Addendum I to Hydrogeologic Characterization Report" which is hereby submitted pursuant to the requirements of Section 10.b of the Facility's RCRA Part B Permit. This report, consisting of two (2) volumes, contains the results of subsurface investigation performed in the fall of 1994, incorporates data obtained from the Wells G&H Superfund Site PRP Group, and supplements the Hydrogeologic Characterization Report which was previously submitted on February 1, 1994.

If you have any questions regarding the technical aspects of this report, please call Jay McCreery at (617) 849-1800, extension 1399.

Very truly yours,

Jules B. Selden Corporate Attorney

Enclosures



Mr. John A. Carrigan Department of Environmental Protection January 31, 1995 Page 2

cc: Charles J. McCreery (enc)
Stephen Applebaum (enc)

Dana Simpson Norman Nelhuebel Joan Murphy (enc)

Joan Murphy (enc)
Woburn Conservation Commission (enc)

#### ADDENDUM I TO HYDROGEOLOGIC CHARACTERIZATION REPORT

Murphy's Waste Oil Service, Inc. 252 Salem Street Woburn, MA 01801

#### **TABLE OF CONTENTS**

INTRODUCTION	1
SITE DESCRIPTION	2
ADJACENT PROPERTIES	3
PREVIOUS CHES INVESTIGATIONS	5
PREVIOUS RETEC INVESTIGATION	6
Surface Samples	6
Subsurface Samples	6 7
Groundwater Samples	8
SCOPE OF WORK	9
CHES SUBSURFACE INVESTIGATION METHODOLOGY	10
Applicable Permits	10
Soil Borings/Monitoring Wells	10
Monitoring Well Installation	12
Wetland Soil Sampling	12
Well Development and Stadia Survey	12
Groundwater Sampling	13
Determination of Aquifer Characteristics	14
Site-Specific Health and Safety Plan	14
CHES SUBSURFACE INVESTIGATION RESULTS	14
Soil Boring Results	14
Field Screening Results	15
Soil Analytical Results	16
Hydrogeologic Observations	17
Aquifer Characteristics	18
Groundwater and Surface Water Analytical Results	18
SUMMARY AND DISCUSSION	19
REFERENCES	22

#### ADDENDUM I TO HYDROGEOLOGIC CHARACTERIZATION REPORT

Murphy's Waste Oil Service, Inc. 252 Salem Street Woburn, MA 01801

### TABLE OF CONTENTS (Continued)

#### **APPENDICES**

Appendix A	Selected Figures from ReTec Report (Ref. 1)
Appendix B	DEP Letter Conditionally Approving Scope of Work
Appendix C	Uniform Hazardous Waste Manifest
Appendix D	Soil Boring Logs and Well Construction Diagrams
Appendix E	Aquifer Test Results
Appendix F	Regional Geologic Maps and Cross-Sections
Appendix G	Soil Analytical Results
Appendix H	Grain Size Analysis
Appendix I	Groundwater and Surface Water Analytical Results



325 WOOD ROAD, P.O. BOX 327 • BRAINTREE, MA 02184-2402 (617) 849-1800 • FAX (617) 849-0812

#### INTRODUCTION

Clean Harbors Environmental Services, Inc. (CHES) has prepared this Addendum I to Hydrogeologic Characterization Report of the property located at 252 Salem Street and 252 Rear Salem Street in Woburn, Massachusetts (the site). The site is owned by Old Oil Realty Trust and is leased by Murphy's Waste Oil Service, Inc. (Murphy's), a transfer, storage and disposal facility for waste oil and solvent-contaminated oil.

This Addendum I to Hydrogeologic Characterization Report was prepared pursuant to the requirements of the RCRA Part B Permit issued by the Massachusetts Department of Environmental Protection (DEP) to Murphy's effective October 19, 1993. Section 10 of the Part B Permit requires a hydrogeologic characterization of the site and site area. An initial Hydrogeologic Characterization Report, dated February 1, 1994, was prepared by CHES and submitted to DEP to document three subsurface investigations which were performed on the site by CHES between December 1987 and February 1989. The Hydrogeologic Characterization Report included results of the previous investigations, a summary of the geology and hydrogeology of the site area, and descriptions of pertinent site features, petroleum use, past spills and a Short-Term Remedial Measure which was performed on the site in March 1989 to remove 1,100 cubic yards of petroleum-contaminated soil during construction of the waste oil facility building and tank farm.

Although the Hydrogeologic Characterization Report satisfied some requirements of the RCRA Part B Permit, additional work was deemed necessary to fulfill all requirements. A Scope of Work for Subsurface Investigation, dated June 30, 1994, was subsequently prepared to address remaining requirements of Section 10.b.1 of the RCRA Part B Permit. The Scope of Work was prepared following review of the report Draft Remedial Investigation, Southwest Properties, Wells G&H Superfund Site, Woburn, Massachusetts (Ref. 1), which was prepared by Remediation Technologies, Inc. (ReTec) for Beatrice Corporation in February 1994. The Murphy's site is located in the southwest corner of the area under investigation for the Central Area Remedial Investigation/Feasibility Study (RI/FS) of the Wells G&H Superfund Site. Some of the information contained in the ReTec report relates to the Murphy's site and was considered

in development of the Scope of Work. The Hydrogeologic Characterization Report and the Scope of Work for Subsurface Investigation were approved by DEP on August 29, 1994.

This Addendum I to Hydrogeologic Characterization Report includes a summary of findings of the ReTec investigation as they relate to the Murphy's site, requirements of the RCRA Part B Permit, and development of the Scope of Work for additional investigation. This report documents results of the additional investigation performed on the site by CHES as proposed in the Scope of Work and addresses remaining requirements of the RCRA Part B Permit.

#### SITE DESCRIPTION

The site is located at 252 Salem Street and 252 Rear Salem Street in the eastern portion of the City of Woburn, Massachusetts. Figure 1 is a Locus Map showing the site location. Properties surrounding the site are shown in Figure 2. The site is located approximately 1,000 feet west of and upgradient from the Aberjona River. The site consists of one parcel of land zoned as industrial and has a total area of approximately 3.4 acres. The City of Woburn Assessor's Office designates the site as Parcel 41, Block 005 on Map 16.

Throughout most of its history, the site has been used primarily as a waste oil and/or virgin oil temporary storage facility. In the 1920s, the Woburn Oil Company reportedly began operations by storing virgin oils on the northern portion of the site. Waste oils were additionally accepted onto the site in the mid-1950s. Murphy's Waste Oil Service, Inc. acquired the site facility on July 7, 1977. As many as 20 aboveground storage tanks installed by Murphy's Waste Oil Service, Inc. were located on the site in 1986. The current owner of the site land is Old Oil Realty Trust, to whom the land was deeded in 1980. In February 1989, Clean Harbors purchased the stock (i.e., the facility and assets) of Murphy's Waste Oil Service, Inc. and has continued to operate the facility under the latter name and leases the land from Old Oil Realty Trust.

The operating portion of the site is surrounded by a chain-link fence which restricts access to the site. Vehicular access to the site is via Salem Street. Figure 3 is a Site Plan illustrating site details. The site is described in three sections, the Northern, Central and Southern Sections. The Northern Section is not paved and is referred to by previous site occupants and on site plans (dated in the 1920s) as the "Oil Yard." A gravel parking area is currently located in the Northern Section of the site. A two-foot high concrete dike, which was constructed in September 1986, is

also located in the Northern Section of the site. The dike surrounded seven aboveground oil storage tanks, which were subsequently relocated to another area of the site in 1990.

The City of Woburn has a sanitary sewer easement across the Northern Section of the site in an east-west orientation. The sewer which traverses the site originates at the westerly abutting property, the former John J. Riley Company tannery, and discharges into a main line of the City of Woburn sanitary sewer system.

The Central Section of the site is occupied by the waste oil facility which contains eleven aboveground storage tanks, an office, a laboratory and a rest room. The facility was constructed between March 1989 and January 1990. The tanks in the facility are located within a concrete containment area which is surrounded by a concrete dike and covered with a canopy. The area surrounding the facility is surfaced with crushed gravel, as is most of the Central Section of the site. Underground utilities which service the oil storage facility include City water and sewer.

A garage is located in the Southern Section of the site. The garage is constructed of steel siding over a four-foot concrete foundation. The floor is also constructed of concrete and does not contain any floor drains. From 1979 to the Summer of 1987, Murphy's Waste Oil Service, Inc. used the garage as an office and for company truck maintenance. The garage is heated by oil which is stored in a 1,000-gallon underground storage tank located off the southeast corner of the building. The areas west and south of the garage are vegetated with grass.

Topographically, the ground surface in the Southern Section of the site slopes down gently to the north from Salem Street. The ground surface is relatively level within the fenced area of the Central and Northern Sections of the site (50 feet National Geodetic Vertical Datum). Properties on Salem Street adjacent to the site are located on high ground, and a steep embankment approximately 30 feet high slopes down to the north outside of the fence. A low wetland area is located outside of the fenced area in the eastern portions of the Central and Northern Sections of the site.

#### ADJACENT PROPERTIES

Properties surrounding the Murphy's site are shown in Figure 2. The Boston and Maine Railroad is adjacent to the west side of the site. Properties west of the railroad tracks include the former

John J. Riley Company tannery (currently a vacant lot and undergoing new site construction) and land currently used as offices and warehouse space for Butterworth/Heinemann Company and other tenants. The adjacent property north of the Murphy's site is undeveloped land owned by the Wildwood Conservation Trust. The land east of Murphy's is an industrial property occupied by Whitney Barrel Company. Three residential properties are located south of the site along Salem Street.

The John J. Riley Company began tannery operations in 1909. The property consisted of one developed parcel (228 Salem Street) with two buildings (a process plant and offices) and an additional undeveloped parcel east of the railroad tracks (referred to here as the Wildwood property). The two parcels of land were sold to Beatrice Foods, Inc. in 1978. In 1983, ownership of the undeveloped parcel was transferred to the Wildwood Conservation Trust.

The John J. Riley tannery was supplied process water from two private wells, one located 110 feet west of the Murphy's site (Production Well No. 1) and one on the Wildwood property 130 feet northeast of Murphy's (Production Well No. 2). The locations of both supply wells are shown in Figure 2. Production Well No. 2 began operation in 1958. Both wells were shut down in 1989 after chlorinated VOCs were identified in groundwater samples from Well No. 2.

Previous site investigations performed at the John J. Riley tannery during the early 1980s identified two chromium and benzidine dye waste lagoons and piles of unprocessed hides north of the process building. Sludge material from process sedimentation tanks were buried next to the lagoons (Ref. 2).

During the early 1980s, miscellaneous debris, piles of rusted 55-gallon drums and pesticide container caps were found on the Wildwood property. Between 200 and 500 five-gallon drums of arsenic trioxide were also found just north of the property (Ref. 2). Based on these findings, the Wildwood property was added to the Wells G&H Superfund Site RI/FS.

Subsequent investigations of the Wildwood property identified surface accumulations of sludge (chemical and petroleum residues), mixed contaminant soils (including polycyclic aromatic hydrocarbon compounds [PAHs], polychlorinated biphenyl compounds [PCBs] and pesticides) and volatile organic compound (VOC) contaminated soils (including trans-1,2-dichloroethene [DCE], trichloroethene [TCE], tetrachloroethene [PCE], 1,1,1-trichloroethane [TCA] and chloroform). Most of the surface accumulations were located directly adjacent to a dirt road

which enters the Wildwood property from Salem Street (through the Aberjona Auto Parts property). Chlorinated VOCs, primarily TCE, have been found to be widely distributed in groundwater on the Wildwood property with the highest concentrations (92,000 micrograms per liter [ug/l]) observed in bedrock fractures (Ref. 3).

The Murphy's site and two other properties north of Salem Street and east of the railroad tracks were added to the Wells G&H Superfund Site investigation in 1989. Murphy's Waste Oil Service, Inc., Whitney Barrel and Aberjona Auto Parts are known as the Southwest Properties of the Central Area which are currently part of the RI/FS. Regional geologic information presented herein was obtained from the ReTec report (Ref. 1) and a subsequent report, Wells G&H Site, Central Area, Remedial Investigation Phase IA Report, which was prepared by GeoTrans, Inc. for Beatrice Corporation in February 1994 (Ref. 4).

#### PREVIOUS CHES INVESTIGATIONS

Based upon the data collected during two structural boring programs and an environmental investigation completed on the Murphy's site between December 1987 and February 1989, the following conclusions were made:

- Groundwater data collected on the site during the period of 1988 through 1989 indicated
  that a persistent plume of chlorinated VOCs existed in groundwater in the Northern
  Section of the site. The presence of this plume was not evident in the Central Section.
  The source of the chlorinated VOCs in groundwater on the site was not identified.
- Chlorinated VOCs were also detected in some soil samples analyzed during the structural boring programs and environmental investigation. Elevated levels of chlorinated VOC contamination were more evident in soil at greater depths.
- Significant petroleum contamination was identified within the Central Section of the site in the area of the new facility. During construction of the new facility, 1,100 cubic yards of petroleum-contaminated soils within the facility footprint were subsequently removed and disposed as a DEP-approved Short-Term Measure.

- A less significant level of petroleum contamination was detected in the Northern Section of the site, west of the diked area.
- The petroleum contamination identified in the site soils appeared to be residual waste oil
  contamination associated with previous site activities. These activities included
  incidental releases and more importantly, historical use of petroleum as dust control and
  historic dumping of petroleum in a waste pit.

#### PREVIOUS RETEC INVESTIGATION

The ReTec report (Ref. 1) documented investigation of the three Southwest Properties, including Murphy's Waste Oil Service, Inc., Whitney Barrel and Aberjona Auto Parts. The ReTec investigation involved sampling and analysis of surface and subsurface soils and groundwater. Figures from the ReTec report showing sample locations and analytical results are presented in Appendix A.

#### Surface Samples

During the ReTec investigation, six surface soil samples were obtained in locations shown with summary sample results in Figures 5-1 through 5-4 in Appendix A. Three of the samples were obtained in the wetland area located between Murphy's Waste Oil and the Whitney Barrel property. Surface soil samples were analyzed for VOCs, semi-volatile organic compounds (SVOCs), PCBs, pesticides, total metals and cyanide.

Analysis of surface soil samples detected chlorinated VOCs, specifically 1,1-DCE and 1,2-DCE, at concentrations up to 4.9 micrograms per kilogram (ug/kg). Gasoline-related VOCs, including benzene, toluene, ethylbenzene and xylenes (BTEX), were detected in two surface soil samples on the Murphy's site at concentrations up to 31.2 ug/kg (Figure 5-1 in Appendix A). Chlorinated VOCs and BTEX compounds were also detected in surface soils at Whitney Barrel and Aberjona Auto Parts at similar concentrations.

PAHs (a sub-class of SVOCs) were detected in surface soil samples on the Murphy's site at total concentrations ranging from 170 ug/kg to 13,964 ug/kg (Figure 5-2 in Appendix A). The highest

levels of PAHs were observed in surface soils at boring MR-2SS, which is located at the northwest corner of the waste oil facility tank farm. The presence of PAHs in this location is attributed to historic soil contamination which was encountered during construction of the building and tank farm. PAHs were also detected in surface soils at Whitney Barrel (up to 11,267 ug/kg) and Aberjona Auto Parts (up to 20,711 ug/kg).

PCB compounds were detected in three surface soil samples collected from the wetland on the Murphy's site at concentrations ranging from 1,096 ug/kg to 13,330 ug/kg (Figure 5-3 in Appendix A). Outside of the wetland, PCBs were detected in surface soils on the Murphy's site only in sample MR-3SS (53 ug/kg), which was obtained at the south end of the concrete dike. PCBs were also detected in surface soils at Whitney Barrel (up to 551 ug/kg) and Aberjona Auto Parts (up to 296 ug/kg). Chlorinated pesticide compounds including endrin and chlordane were also detected in the wetland surface soil samples on the Murphy's site at total concentrations ranging up to 2.89 milligrams per kilogram (mg/kg). These compounds were detected in surface soils outside of the wetland on the Murphy's site at total concentrations up to 0.08 mg/kg. Endrin and chlordane were detected in surface soils at Whitney Barrel at total concentrations up to 1.39 mg/kg.

Elevated concentrations of some metals, including arsenic (up to 17.0 mg/kg), cadmium (up to 4.8 mg/kg), chromium (up to 8,193 mg/kg) and lead (up to 1,245 mg/kg), were detected in the three surface soil samples from the wetland on the Murphy's site, with the highest concentrations observed in sample MR-SS7 which was obtained at the northeast corner of the site (Figure 5-4 in Appendix A). Relatively low concentrations of these metals were detected in surface soil samples collected outside of the wetland on the Murphy's site. Cyanide was also detected in two of the wetland samples at concentrations up to 4.7 mg/kg. Cyanide was not detected in surface soils elsewhere on the Murphy's site, however, low concentrations of cyanide below the Practical Quantitation Limit (PQL) were detected in surface soils at Whitney Barrel.

#### Subsurface Samples

During the ReTec investigation, four subsurface soil samples were obtained on the Murphy's site at locations shown with summary sample results in Figures 5-5 through 5-8 in Appendix A. Subsurface soil samples were obtained at the groundwater interface (approximately three to four feet below grade) and analyzed for VOCs, SVOCs, PCBs, pesticides, total metals and cyanide.

Elevated concentrations of VOCs were detected in subsurface sample MR-SS2D, which is located at the northwest corner of the waste oil facility tank farm (Figure 5-5 in Appendix A). Chlorinated VOCs, including 1,2-DCE and TCE, were detected in the sample at a total concentration of 3,633 ug/kg; BTEX compounds were detected at a total concentration of 15,311 ug/kg. Concentrations of chlorinated VOCs and BTEX compounds in other subsurface samples obtained at Murphy's, Whitney Barrel and Aberjona Auto Parts were comparatively low.

PAHs were detected in subsurface sample MR-SS2D at a total concentration of 3,745 ug/kg and are attributed to historic soil contamination which was encountered during construction of the waste oil facility building and tank farm (Figure 5-6 in Appendix A). PAHs were otherwise not detected in subsurface soils on the Murphy's site. Elevated concentrations of PAHs were detected in subsurface soils at Whitney Barrel (up to 21,686 ug/kg).

PCBs were not detected in subsurface soils at any of the four sampling locations on the Murphy's site (Figure 5-7 in Appendix A). PCBs were detected in subsurface soils at Whitney Barrel (up to 1,414 ug/kg) and Aberjona Auto Parts (515 ug/kg). Pesticides were detected in subsurface soils on the Murphy's site at total concentrations up to 0.20 mg/kg and at Whitney Barrel at total concentrations up to 0.23 mg/kg.

Metals were detected in subsurface soils at the Murphy's site at levels which were typical of most other subsurface samples obtained at Whitney Barrel and Aberjona Auto Parts (Figure 5-8 in Appendix A). Moderate concentrations of cadmium (1.2 mg/kg) and lead (485 mg/kg) were detected in sample MR-SS2D obtained at the northwest corner of the waste oil facility tank farm, and are attributed to historic soil contamination. Cyanide was not detected in any of the subsurface soil samples obtained on the Murphy's site.

#### **Groundwater Samples**

During the ReTee investigation, groundwater samples were obtained from two monitoring wells on the Murphy's site in locations shown with summary sample results in Figures 5-9 and 5-10 in Appendix A. Both of the wells are screened across the water table to monitor water quality in the upper portion of the aquifer. Well MR-1SS is located in the northern portion of the site near the concrete dike and adjacent to the sewer line; well MR-2SS is located at the northwest corner of

the waste oil facility tank farm (see Site Plan, Figure 3). Groundwater samples were analyzed for VOCs, SVOCs, PCBs, pesticides, dissolved metals and cyanide.

Chlorinated VOCs, including 1,1 dichloroethane (DCA), 1,1,1-TCA, PCE and TCE were detected in groundwater from well MR-1SS at a total concentration of 11.5 ug/l; chlorinated VOCs (primarily 1,2-DCE) were detected in well MR-2SS at a total concentration of 483.6 ug/l (Figure 5-9 in Appendix A). Gasoline-related BTEX compounds were also detected in well MR-2SS at a total concentration of 345.5 ug/l.

Low concentrations of SVOCs were detected in groundwater from well MR-2SS, including the PAHs naphthalene (21 ug/l), 2-methylnaphthalene (19 ug/l), and pyrene (3 ug/l). PAHs were not detected in groundwater from well MR-1SS.

Analysis of groundwater samples from wells MR-1SS and MR-2SS by ReTec did not detect any PCB or pesticide compounds.

Dissolved lead (0.029 milligrams per liter [mg/l]) and zinc (0.025 mg/l) were detected in groundwater from well MR-2SS (Figure 5-10 in Appendix A). No other dissolved metals or cyanide were detected in groundwater samples from the two wells.

#### SCOPE OF WORK

In order to satisfy the requirements of the RCRA Part B Permit for the Murphy's facility, a Scope of Work for Subsurface Investigation, dated June 30, 1994, was submitted to DEP. The Scope of Work included the following proposed tasks:

- installation of new groundwater monitoring wells on the site upgradient and downgradient of the waste oil facility building, including one deep well to be continued to the lower-boundary of the uppermost aquifer;
- collection, characterization and field-screening of samples from the soil borings, and laboratory analysis of select samples;

- collection of surface soil samples from the wetland on the east side of the site for laboratory analysis;
- collection and laboratory analysis of groundwater samples from new and existing wells on the site, and surface water from the wetland on the east side of the site;
- determination of aquifer characteristics at each well location using a rising-head slug test;
   and
- documentation of findings of the subsurface investigation in a report with other regional information.

The Scope of Work was approved by DEP in a letter dated August 29, 1994 (Appendix B) with minor modifications which were incorporated into the investigation.

#### CHES SUBSURFACE INVESTIGATION METHODOLOGY

#### **Applicable Permits**

Prior to drilling, the locations of all known subsurface utilities were determined and DIGSAFE was notified. Since drilling was proposed within 100 feet of the wetland, a Request for Determination of Applicability of the Woburn Wetlands Ordinance was filed with the City of Woburn Conservation Commission. The Conservation Commission determined that the Wetlands Ordinance was not applicable to the planned drilling operations.

#### Soil Borings/Monitoring Wells

Seven groundwater monitoring wells were installed on the site during the period of October 12-18, 1994 by Environmental Drilling, Inc. in locations shown on Figure 3 (Site Plan). Wells MW-1 and MW-2 were installed along the west site boundary; wells MW-3, MW-4 and MW-5S were installed east of the dike wall and facility building adjacent to the wetland; well MW-6 was installed southeast of the waste oil facility building. One deep well (MW-5D) was installed east of the facility building adjacent to shallow well MW-5S. Soil borings for wells MW-1, MW-2,

MW-3, MW-4, MW-5S and MW-6 were continued to depths of 15 to 20 feet below grade; deep well MW-5D was continued to bedrock refusal at 83 feet below grade.

Soil borings for the shallow wells were performed using 41/4-inch hollow-stem auger. Boring MW-5D was installed using drive and wash methodology. Soil samples were collected continuously in the shallow borings; samples were collected at a five-foot interval in boring MW-5D below the zone characterized in adjacent boring MW-5S. The soil borings were performed in accordance with ASTM D1586, "Penetration Test and Split Barrel Sampling of Soils." Soil samples were obtained using a two-inch diameter split-spoon sample tube advanced ahead of the auger (or driven casing) according to a standard penetration test using a 30-inch drop from a 140-pound hammer. Hollow-stem auger was decontaminated by steam prior to each soil boring. Split-spoon sample tubes were washed with Liquinox detergent and then rinsed with methanol and deionized water. Drill cuttings were containerized for later characterization and proper disposal. The Uniform Hazardous Waste Manifest for disposal of soil cuttings generated during this investigation is presented in Appendix C.

All soil samples were visually described noting grain size, apparent water saturation, and color. Soil boring logs containing sample descriptions and other pertinent information are presented in Appendix D. All soil samples were split vertically and prepared for field-screening and laboratory analysis. Samples for field-screening were placed in clean 16-ounce glass jars and covered with aluminum foil prior to replacing the lid. Samples for laboratory analysis were transferred into clean glass jars with Teflon-lined lids and stored in a cooler.

Soil samples for field-screening were allowed to equilibrate for a minimum of 15 minutes for headspace development, and then were screened using a flame ionization detector (Foxboro Model 128 Organic Vapor Analyzer [OVA]). This instrument measures the total VOCs in vapor and reports in terms of parts per million (ppm) referenced to methane. Total VOC headspace measurements are presented in the soil boring logs and are summarized in Table 1.

Based on results of field-screening and/or evidence of possible soil staining, select samples from the borings were laboratory-analyzed for VOCs (by EPA Method 8260), SVOCs (by EPA Method 8270), total petroleum hydrocarbons (TPH by GC/FID), PCB/pesticide compounds (by EPA Method 8080), 13 priority pollutant total metals and total cyanide. In each of the shallow borings, a soil sample was obtained from the surface interval (0 - 2 feet below grade) for laboratory analysis of TPH. In addition to analytical testing, one soil sample from each of the

borings was composited over the screened interval for determination of grain size distribution by sieve analysis (by ASTM Method D422).

#### Monitoring Well Installation

The seven soil borings were completed with installation of groundwater monitoring wells. The wells were constructed of two-inch diameter Schedule 40 flush-joint threaded polyvinyl chloride (PVC) factory slotted (0.01-inch) well screen. The shallow wells were screened across the groundwater table in the upper aquifer; deep well MW-5D was screened at the bedrock surface at the lower boundary of the aquifer. The annular space around the well screen was packed with #2 silica sand to a depth of approximately one foot above the top of the well screen. A subsurface seal of at least one foot of bentonite was placed above the sand pack. The shallow wells were backfilled to grade with Portland cement; deep well MW-5D was backfilled with powdered bentonite/cement grout conveyed through a tremie tube. Locking guard pipes were installed over all of the wells and protective bumper posts were installed adjacent to the guard pipes in traffic areas. Schematic construction diagrams for the monitoring wells are presented in Appendix D.

#### Wetland Soil Sampling

Soil samples were obtained on October 13 - 14, 1994 in four locations at the edge of the wetland area, designated as SW-1, SW-2, SW-3, and SW-4 (Figure 3). In each location, a grab sample was obtained of the upper six inches of wetland soils. Samples from each location were laboratory-analyzed for VOCs, SVOCs, TPH, PCB/pesticides, 13 priority pollutant metals and total cyanide. Wooden stakes were placed at each of the locations so they could be reoccupied for water sampling.

#### Well Development and Stadia Survey

All of the wells were developed on October 31, 1994 using a surface pump. Groundwater was purged from each well until clear. A slow pumping rate was used to avoid de-watering of the screened interval. Purged groundwater was containerized for characterization and proper disposal. Based on the results of the analytical data, the purged groundwater was batched

together with other oily wastewater from the Murphy's oil recycling facility and shipped off-site for proper treatment and disposal.

A stadia survey was performed on October 31, 1994 to determine the well rim elevations to the nearest one-hundredth of a foot relative to the National Geodetic Vertical Datum of 1929. Wooden reference stakes placed in the wetland were also surveyed for use in measuring surface water elevations.

#### **Groundwater Sampling**

The newly-installed wells and existing wells MR-1SS and MR-2SS (installed during the ReTec investigation) were sampled on November 9, 1994. Prior to purging the wells, water level was measured in each of the wells and surface water location SW-3. Surface water was not present at locations SW-1, SW-2 and SW-4 in the wetland at the time of sampling. After measurement of water levels, the wells were purged by removal of at least three casing volumes of groundwater to assure that representative samples were obtained. Field measurements were then recorded in each of the locations for pH, temperature and specific conductance.

Water samples from each of the wells were obtained using pre-cleaned Teflon bailers; surface water samples at location SW-3 were obtained by direct filling of the sample containers. Groundwater and surface water samples were laboratory-analyzed for VOCs (by EPA Method 624), SVOCs (by EPA Method 625), TPH (by GC/FID), PCB/pesticide compounds (by EPA Method 608), 13 priority pollutant dissolved metals and total cyanide. In addition, a trip blank was prepared to accompany the sample jars to and from the site which was analyzed with the other samples for VOCs.

Installation of monitoring wells and sampling was performed in accordance with DEP Policy #WSC-310-91, *Standard References for Monitoring Wells*. All analyses were performed by CHES' laboratory in Braintree, Massachusetts (Massachusetts Registration No. M-MA00032).

#### **Determination of Aquifer Characteristics**

Hydraulic conductivity was measured in new and existing wells on the site on November 21, 1994 using a rising-head slug test. To conduct the test, a weighted slug was lowered into each of monitoring wells to displace water upward in the well. After equilibration of the water level, the slug was withdrawn and recovery of the water level was recorded utilizing a pressure transducer and environmental data logger (In-Situ Model SE-1000B). Vertically-averaged values of hydraulic conductivity over the screened interval in each well were calculated by the Hvorslev Method. Results of the aquifer testing are presented in Appendix E and are summarized in Table 2.

#### Site-Specific Health and Safety Plan

All operations associated with the investigation were performed by workers specifically trained in the handling of hazardous materials under OSHA regulations at 29 CFR 1910.120. All safety equipment and work procedures were conducted in accordance with a site-specific Health and Safety Plan. The Health and Safety Plan included specifications of the level of personal protection, designation of work zones and decontamination procedures.

#### CHES SUBSURFACE INVESTIGATION RESULTS

#### Soil Boring Results

Shallow soil types encountered during installation of wells MW-1 through MW-6 consisted of approximately eight feet of fill material, including fine to coarse sand with little silt and gravel, overlying native sand with varying amounts of gravel. The transition from fill to native materials was not readily apparent in most of the borings because native materials were used to fill the property. The transition was most clear in boring MW-3, in which a thin (two-inch) layer of peat was noted at the contact. The peat was encountered in MW-3 at a depth of 7.5 feet below grade and is presumed to represent wetland deposits which were covered by fill during site construction. A geologic cross-section oriented north-south through the site is shown in Figure 4 which shows the spatial relationship of the fill material to the wetland.

Appendix F contains regional maps and cross-sections from the ReTec and GeoTrans reports which are pertinent to the site. Figure 3-2 in Appendix F is a Surficial Geologic Map of the Wells G&H Central Area adjacent to the site. Although coverage on the map does not extend to the Murphy's site, the map shows that Aberjona Auto Parts and Whitney Barrel are located on filled land within the Aberjona River Basin similar to Murphy's.

The native sand and gravel aquifer was penetrated by the soil boring for well MW-5D, which was continued to refusal at a depth of 83 feet below grade. The lower portion of the aquifer consisted of well-sorted fine sand with little to no gravel. A confining layer marking the lower boundary of the aquifer was not reached prior to refusal, which was presumed to be the bedrock surface. A ten-foot well screen was used in well MW-5D due to the anticipated slow groundwater recharge from the fine sands.

Refusal was encountered in boring MW-5D at a depth which was slightly deeper than the anticipated depth to bedrock, based on a regional cross-section presented in the ReTec report. Figure 4-4 in Appendix F shows the regional cross-section which has been modified to show the depth at which refusal was encountered in boring MW-5D. The location of the cross-section is shown in Figure 4-3 in Appendix F. A Bedrock Contour Map presented in Figure 4-6 in Appendix F indicates the bedrock surface underlying the site slopes down to the southeast. The Bedrock Contour Map presented in Figure 4-6 agrees closely with the depth at which refusal was encountered in boring MW-5D.

#### Field-Screening Results

Field-screening headspace measurements are shown on the soil boring logs and are summarized in Table 1. Profiles of field-screening results (in ppm) with depth in each of the borings are presented in Figure 5. Headspace measurements of soil samples obtained from borings MW-1, MW-5S, MW-5D and MW-6 were less than 10 ppm. Elevated measurements were obtained during field-screening of samples from borings MW-2 (to greater than 1,000 ppm), MW-3 (up to 460 ppm) and MW-4 (up to 92 ppm). Elevated headspace measurements in boring MW-2 were observed in shallow samples (0 - 6 feet below grade) and are attributed to the presence of VOCs in the unsaturated fill material. In contrast, the maximum headspace measurements in borings MW-3 and MW-4 were observed at depth (10 - 12 feet below grade) in saturated samples below the water table. These elevated headspace measurements are attributed to methane from the

adjacent wetland. A hydrogen sulfide odor was noted in soil samples obtained below the groundwater table in both borings MW-3 and MW-4.

#### Soil Analytical Results

Analytical results of the soil boring samples are presented in Appendix G and are summarized in Tables 3, 4 and 5. Low concentrations of acetone (210 ug/kg) and 2-butanone (50 ug/kg) were detected in shallow soils (2 - 4 feet below grade) in boring MW-2 (Table 3), in which elevated headspace measurements were obtained in the same depth interval. A low concentration of acetone (23 ug/kg) was also detected in one soil sample from boring MW-4 below the water table at a depth of 10 to 12 feet below grade. VOCs were detected in only one of the four wetland soil samples obtained on the site. Xylenes were detected at a concentration of 1,300 ug/kg in sample SW-2. VOCs were not detected in any of the other soil boring or wetland samples.

Fluoranthene, a PAH compound, was detected in one surface soil sample (0 - 2 feet below grade) from boring MW-6 at a concentration of 3,300 ug/kg (Table 4). Soil in this sample was stained black and contained a trace of brick debris. Fluoranthene was also detected in surface soils in the wetland at location SW-1 (640 ug/kg) and SW-4 (2,000 ug/kg). Other SVOCs which were detected in wetland samples SW-1 and SW-4 include the PAHs benzo(b)fluoranthene (up to 2,000 ug/kg), benzo(a)pyrene (340 ug/kg), and pyrene (430 ug/kg).

TPH was detected at concentrations ranging from non-detectable levels up to 470 mg/kg in the soil boring samples (Table 4). TPH was detected in the wetland soil samples at concentrations from 72 mg/kg (at SW-1) to 97,000 mg/kg (at SW-2). PCB compounds were also detected in wetland samples SW-2 (220 mg/kg), SW-3 (15 mg/kg) and SW-4 (0.8 mg/kg). PCBs detected in the wetland samples were of two different types. Aroclor 1254 was detected at locations SW-2 and SW-3; Aroclor 1260 was detected at location SW-4. Organochlorine pesticide compounds were not detected in any of the soil boring or wetland samples obtained during this investigation.

Low concentrations of the 13 priority pollutant total metals were detected in the soil boring samples obtained during this investigation (Table 5). Elevated concentrations of some metals were detected in the wetland soil samples, including antimony (up to 80 mg/kg), chromium (up to 5,700 mg/kg), lead (up to 35,100 mg/kg) and zinc (up to 5,200 mg/kg). The highest concentrations of metals were observed at location SW-2. Low concentrations of total cyanide

were also detected in wetland soil samples SW-1 (2.2 mg/kg) and SW-2 (3.6 mg/kg). Cyanide was not detected in any of the other soil boring or wetland samples obtained during this investigation.

#### **Hydrogeologic Observations**

Groundwater and surface water elevations measured on the site on November 9 and December 13, 1994 are presented with other field data in Tables 6 and 7, respectively. The depth to groundwater on the site was observed to vary from five to eight feet below grade in the Northern and Central Sections of the site and up to ten feet below grade in the Southern Section. The data indicate that the groundwater and surface water levels were up to 1.7 feet higher during the December 13 sample event. A portion of the rise in water levels is attributed to a storm over the period of December 10 - 11, which resulted in 0.7 inch of rain (precipitation data supplied by National Weather Service, Logan International Airport, Boston, Massachusetts).

Groundwater contour plans constructed using elevation data collected on November 9, 1994 and December 13, 1994 are presented in Figures 6 and 7, respectively. Both contour plans show a very low hydraulic gradient across the site. During the November sample event, water elevations varied by up to 0.36 foot and no distinct horizontal hydraulic gradient (groundwater flow direction) was observed. Water levels in December were higher and a low hydraulic gradient (0.18%) to the south had developed, with variation in observed water elevations up to 0.55 feet. Regional groundwater contour plans presented in the ReTec report (Figures 4-7 and 4-8 in Appendix F) also show a very low horizontal hydraulic gradient in the site area. The groundwater level in well MR-1SS appeared to be anomalously low compared to other wells on the site during both monitoring events. Well MR-1SS is located directly adjacent to the sewer line which traverses the site and may not be representative of actual groundwater levels.

The vertical hydraulic gradient on the site was calculated using groundwater elevation data from wells MW-5S and MW-5D. During the November sample event, a downward (negative) vertical hydraulic gradient of - 0.50% was measured. A similar value (- 0.53%) was measured during the December monitoring event.

#### Aquifer Characteristics

Rising-head slug tests yielded an average value of hydraulic conductivity of  $3.3 \times 10^{-2}$  centimeter per second (cm/sec) in shallow wells screened in the fill material and the underlying native soils which is a typical value for clean sand (Ref. 5). Well MW-6 yielded the highest value of hydraulic conductivity (8.7 x  $10^{-2}$  cm/sec), indicating the coarsest material. Well MW-3 yielded the lowest value (1.0 x  $10^{-2}$  cm/sec) of the newly-installed shallow wells. The slug test data for deep well MW-5D yielded a value of  $1.9 \times 10^{-4}$  cm/sec, which is a typical value for silty sand.

Results of grain size analyses of composite soil samples obtained from the screened interval in each of the new borings are presented in Appendix H. These data were consistent with visual observations made during drilling and with soil types predicted by the slug test data. Based on the grain size analyses, soil samples from the screened interval in the shallow borings are characterized as poorly-sorted sand with up to 60% fine gravel and less than 10% silt and clay. The sample from boring MW-6 contained the highest percentage of coarse material; samples from MW-3 and MW-4 yielded the lowest percentage of coarse material in the shallow borings. Significantly finer material was indicated in the sample from deep boring MW-5D, which contained 35% poorly-sorted sand and 65% silt and clay.

The average linear velocity of groundwater flow at each well was calculated using measured values of hydraulic conductivity and hydraulic gradient and an assumed value of effective porosity of the soil matrix (25%). Using these values, the average horizontal linear velocity in the shallow aquifer was  $9.9 \times 10^{-11}$  foot per day (ft/d). The average vertical linear velocity is  $7.0 \times 10^{-10}$  ft/d in the upper aquifer and  $1.5 \times 10^{-12}$  ft/d in the lower aquifer. As such, groundwater flow on the site is considered to be nearly stagnant. Calculated values of average linear velocity are listed in Table 2.

#### Groundwater and Surface Water Analytical Results

Analytical results of the groundwater and surface water samples obtained during this investigation are presented in Appendix I and are summarized with previous data in Tables 8, 9 and 10. VOCs were detected only in shallow wells MW-3, MR-1SS and MR-2SS (Table 8). Chlorinated VOCs, including trans,1-2-DCE, TCE, 1,1-DCA and 1,1,1-TCA, were detected in well MW-3 at a total concentration of 1,342 ug/l. Trans-1,2-DCE was the primary VOC detected

in well MW-3 (1,100 ug/l). Trans-1,2-DCE was also detected in well MR-2SS (240 ug/l), which is located adjacent to the facility tank farm. Other VOCs detected in well MR-2SS during this investigation included vinyl chloride (15 ug/l) and the gasoline-related BTEX compounds benzene, toluene and xylenes (each 9 ug/l). No VOCs were detected in deep well MW-5D or the surface water sample obtained in the wetland at location SW-3.

.

Di-n-butylphthalate, an SVOC, was detected in groundwater in wells MW-6, MR-1SS and MR-2SS and in surface water sample SW-3 at concentrations ranging from 12 ug/l to 220 ug/l. Di-n-butylphthalate was not detected in any of the soil samples collected during the investigation. Di-n-butylphthalate is a plasticizer which is not normally associated with petroleum products. Plastics used in underground utility lines on the site may be one possible source of the compound. No other SVOCs were detected in groundwater or surface water on the site. PCBs and organochlorine pesticide compounds were not detected in any of the groundwater or surface water samples (Table 9). TPH was detected in each of the samples at very low concentrations (up to 3.4 mg/l).

Dissolved metals, including antimony, arsenic, cadmium, lead, and zinc, were detected in groundwater samples from several of the wells at concentrations equal to or just above the PQLs (Table 10). Dissolved lead was detected in well MR-2SS at a slightly higher concentration (up to 0.029 mg/l). Dissolved lead was also detected in surface water sample SW-3 at a concentration of 0.028 mg/l. Total cyanide was not detected in any of the groundwater or surface water samples.

#### SUMMARY AND DISCUSSION

This Addendum I to Hydrogeologic Characterization Report was prepared to satisfy requirements stipulated in the RCRA Part B Permit for Murphy's Waste Oil Service, Inc. in Woburn, Massachusetts and includes a characterization of the geology and hydrogeology of the site. This report includes a summary of findings of previous subsurface investigations performed at the site and documents results of the current investigation which was performed by CHES between September and November 1994.

Previous subsurface investigations performed by CHES between December 1987 and February 1989 identified oil-impacted soil in two areas of the Murphy's site. TPH was detected in shallow

soils (2 - 4 feet below grade) at concentrations up to 16,000 mg/kg in the Northern Section of the site where aboveground oil storage tanks were formerly located. TPH concentrations up to 21,000 mg/kg were also detected in soils in the Central Section of the site in the area of the former oil pit. 1,100 cubic yards of oil-contaminated soils were subsequently removed from the Central Section of the site as a Short-Term Measure during construction of the new waste oil facility building in 1989. In 1994, a subsurface investigation of the site area performed by ReTec identified PAHs in soil adjacent to the Murphy's facility building at concentrations up to 9,087 ug/kg, indicating that some residual oil-impacted soils remained after implementation of the Short-Term Measure.

The ReTec investigation also identified impacted soils in the wetland between the Murphy's site and Whitney Barrel, which were found to contain PAHs (up to 6,162 ug/kg), pesticides (up to 2.89 mg/kg), arsenic (up to 17.0 mg/kg), cadmium (up to 4.8 mg/kg), chromium (up to 8,193 mg/kg), and cyanide (up to 4.7 mg/kg). Analytical results obtained during the current CHES investigation confirmed the ReTec results, and detected TPH (up to 97,000 mg/kg), VOCs (up to 1,300 ug/kg), PCBs (up to 220 mg/kg), and lead (up to 35,100 mg/kg) in the wetland soils. Analytical results obtained during the ReTec investigation and the current investigation did not suggest an on-site source of contaminants in the wetland soils. Elevated concentrations of PCBs, pesticides, metals and cyanide were not detected elsewhere on the Murphy's site outside the wetland during either of the investigations. Of the contaminants identified in the wetland, only low concentrations of TPH (up to 470 mg/kg), and chromium (up to 4.9 mg/kg) were identified in adjacent borings MW-3, MW-4 and MW-5S.

During the current subsurface investigation, horizontal and vertical hydraulic gradients on the site were observed to be very low. Although shallow soils (less than 20 feet) were found to consist of relatively coarse sand and gravel, the low measured hydraulic gradients indicate that groundwater flow on the site is nearly stagnant. Since the vertical hydraulic gradient on the site was observed to be slightly greater and more persistent than the horizontal gradient, a very slow net groundwater flow downward is anticipated.

Prior to 1989, groundwater flow on the site was likely influenced by the John J. Riley Company Production Wells No. 1 (depth unknown) and No. 2 (screened from 36 to 51 feet below grade). Only one private water supply well is known to exist in the site area. A shallow well is located at Woburn Concrete Products approximately  $\frac{1}{4}$ -mile south of the site (Figure 2). The well, which was installed approximately 30 years ago, is screened at an estimated depth of 40 feet below

grade and is currently used for mixing concrete only. It is not anticipated that this well influences groundwater flow on the Murphy's site.

Analytical data collected on the site during the current investigation detected chlorinated VOCs in shallow groundwater in the Northern Section of the site. Elevated concentrations of chlorinated VOCs, including trans-1,2-DCE, TCE, 1,1-DCA and 1,1,1-TCA were detected in well MW-3 in the Northern Section of the site at a total concentration of 1,342 ug/l. Elevated concentrations of chlorinated VOCs were also detected in the Northern Section during the previous subsurface investigation performed by CHES (Ref. 6). The source of chlorinated VOCs in shallow groundwater in the Northern Section of the site has not been determined. Analytical data collected during this investigation and previous investigations performed by ReTec and CHES have not detected chlorinated VOCs in soils above the groundwater table on the site at concentrations which would indicate a source area.

Chlorinated VOCs were also detected in shallow groundwater adjacent to the facility tank farm. Trans-1,2-DCE and vinyl chloride were detected in well MR-2SS adjacent to the tank farm at a total concentration of 255 ug/l. The origin of VOCs at well MR-2SS is unknown, however, analytical data from other shallow wells do not suggest widespread occurrence of chlorinated VOCs in groundwater between wells MR-2SS and MW-3.

Groundwater quality in the lower portion of the aquifer was evaluated in deep well MW-5D. The lower boundary of the aquifer was found to be the bedrock surface, which was encountered at a depth of 83 feet below grade. Well MW-5D was screened at the bedrock surface in a location which is structurally down-dip from the waste oil facility building and tank farm (Figure 4-6 in Appendix F). Except for TPH (detected at 0.2 mg/l), groundwater analyses from well MW-5D did not indicate the presence of any contaminants which have been observed in shallow groundwater on the site.

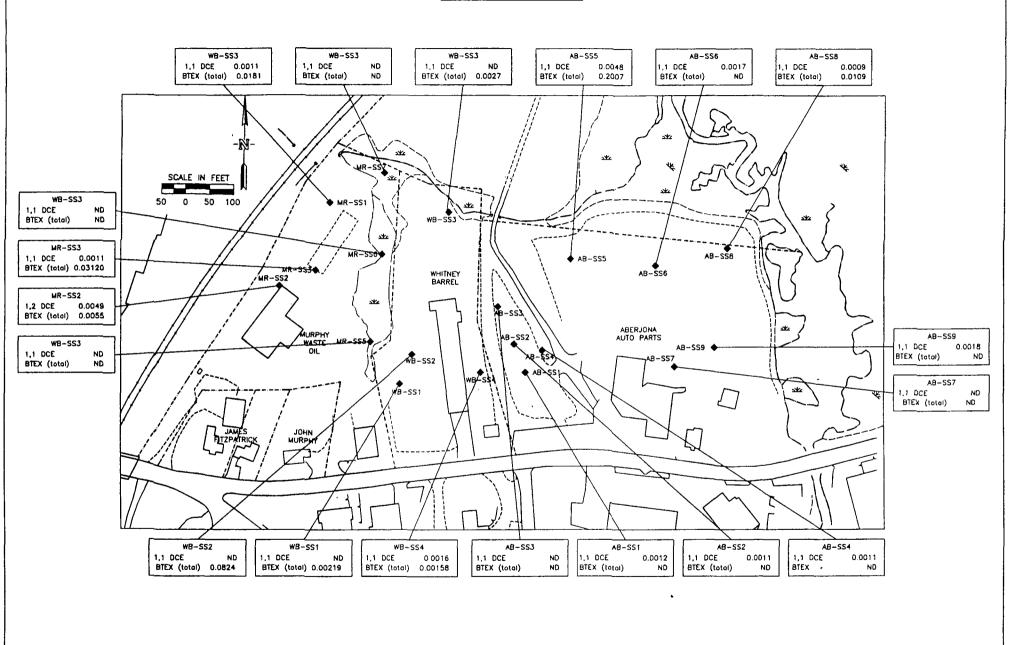
3351 Text (Rev. 01)

#### REFERENCES

- 1. Draft Remedial Investigation, Southwest Properties, Wells G&H Superfund Site, Woburn, Massachusetts, by Remediation Technologies, Inc., February 1994.
- 2. Wells G&H Site Remedial Investigation Report, NUS Corporation, Superfund Division, October 17, 1986.
- 3. Draft Predesign Investigation Report, Wildwood Property, Wells G&H Superfund Site, Woburn, Massachusetts, by Remediation Technologies, Inc., March 1993.
- 4. Wells G&H Site, Central Area, Remedial Investigation Phase IA Report, by GeoTrans, Inc., February 1994.
- 5. Freeze, R.A. & J.A. Cherry, "Groundwater." Prentice-Hall, Inc. 1979.
- 6. Hydrogeologic Characterization Report, Murphy's Waste Oil Service, Inc., by Clean Harbors Environmental Services, Inc., February 1994.

# APP. A





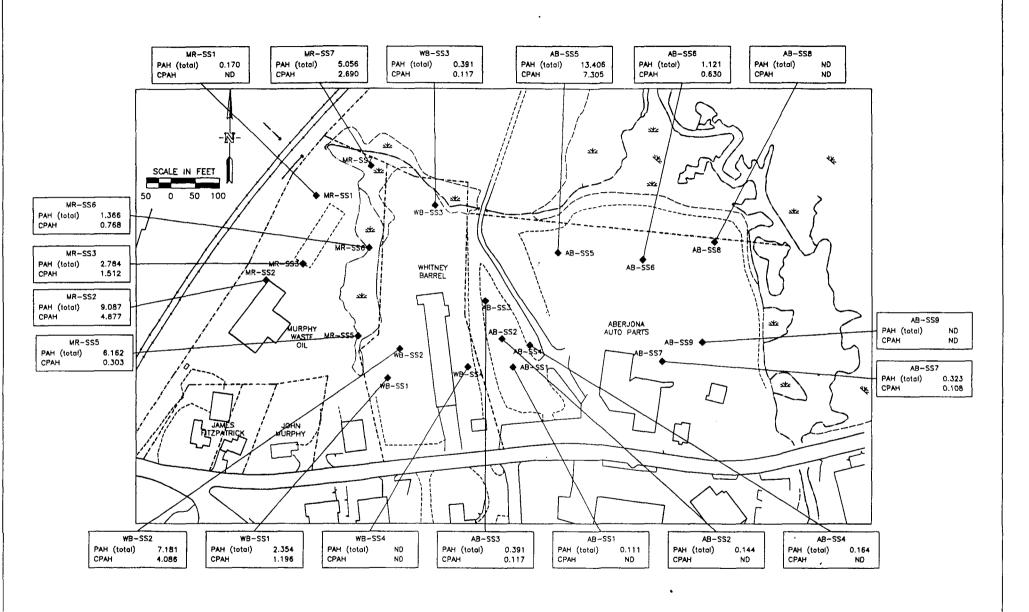
FIGURE

5-1

0681S003

SURFACE SOIL VOC RESULTS
All Values are in mg/kg



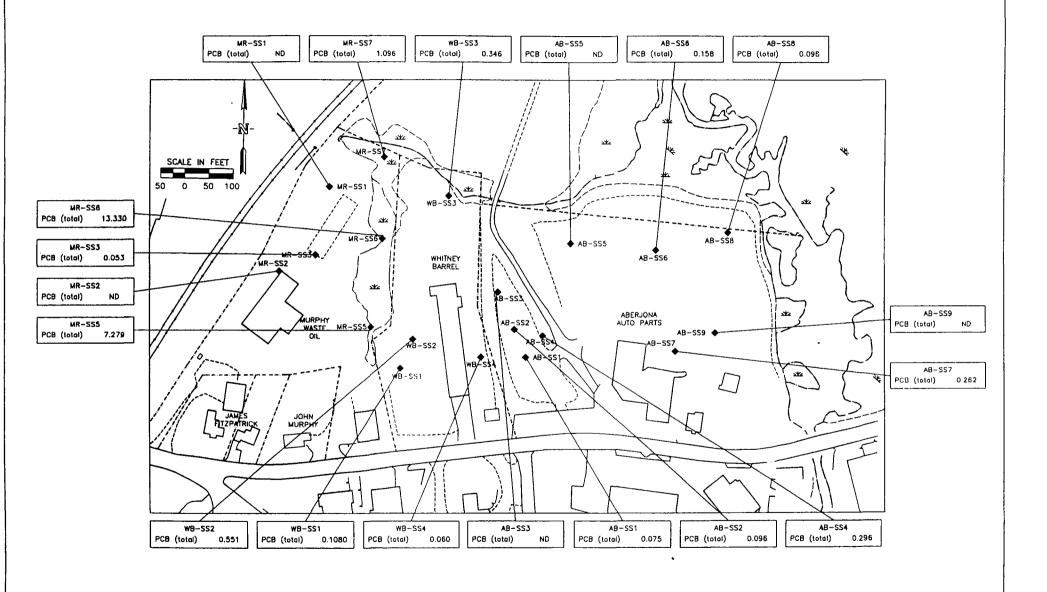


06815003

SURFACE SOIL SVOC RESULTS
All Values are in mg/kg

FIGURE **5-2** 



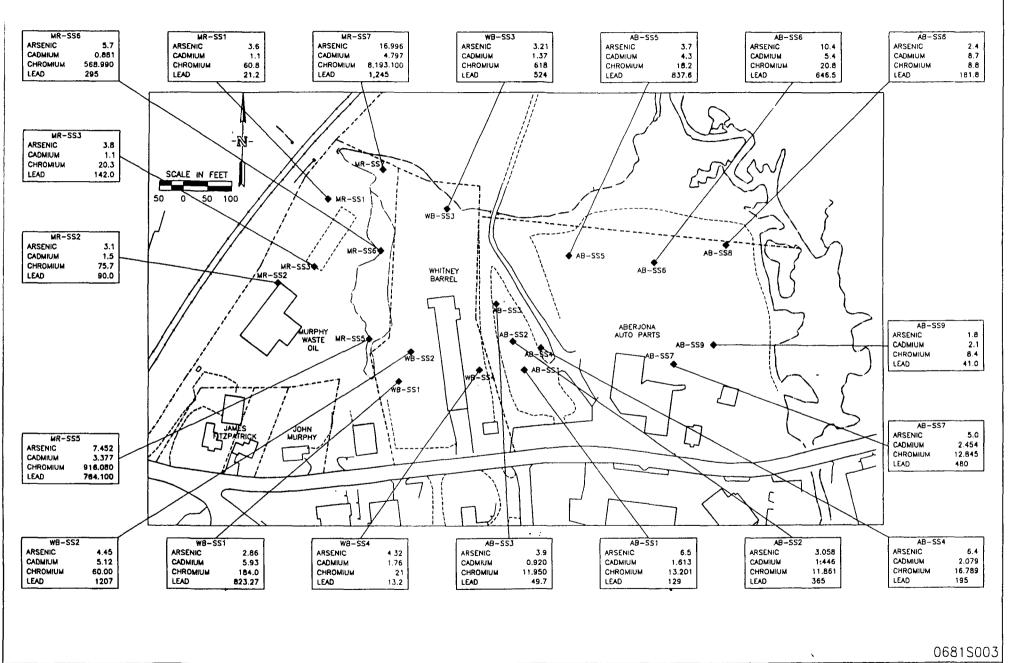


0681S003

SURFACE SOIL PCB RESULTS
All Values are in mg/kg

FIGURE

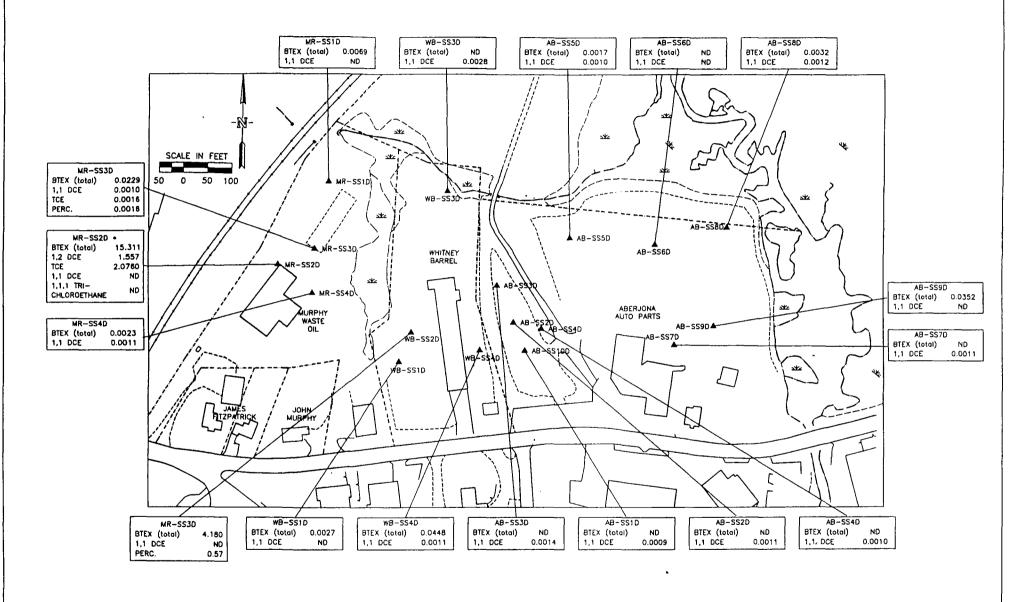
## REFOC



SURFACE SOIL METALS RESULTS
All Values are in mg/kg

FIGURE





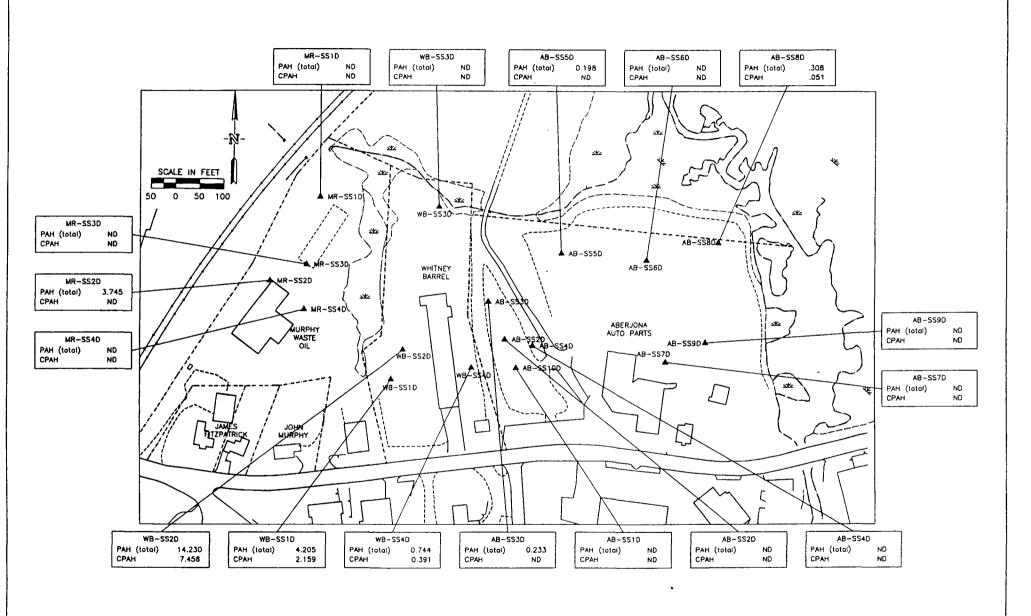
. 1,2 DCE & TCE Not detected except as noted

06815003

SUBSURFACE SOIL VOC RESULTS
All Values are in mg/kg

FIGURE



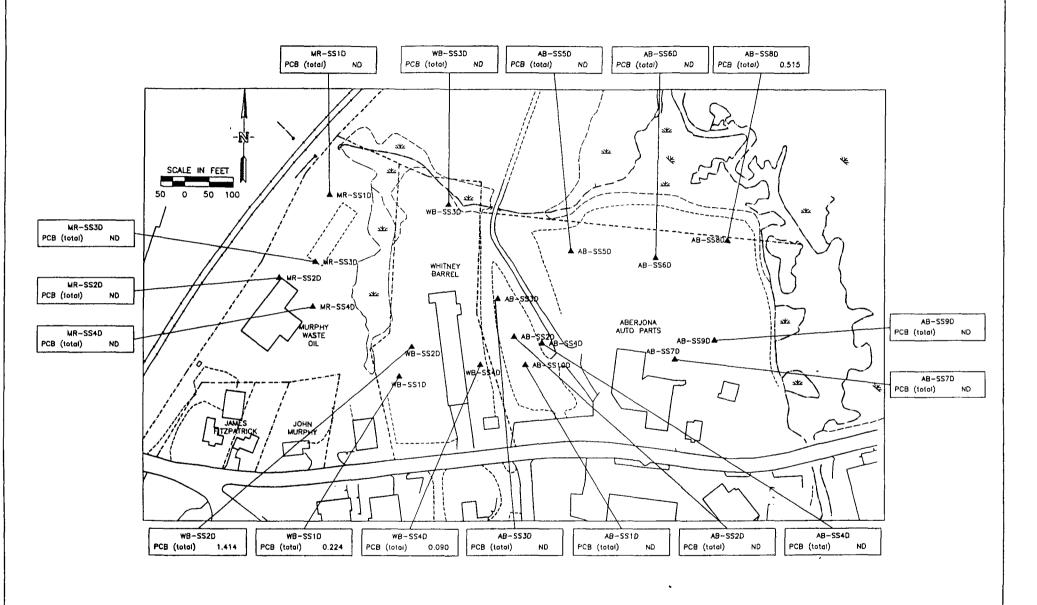


06815003

SUBSURFACE SOIL SVOC RESULTS
All Values are in mg/kg

FIGURE



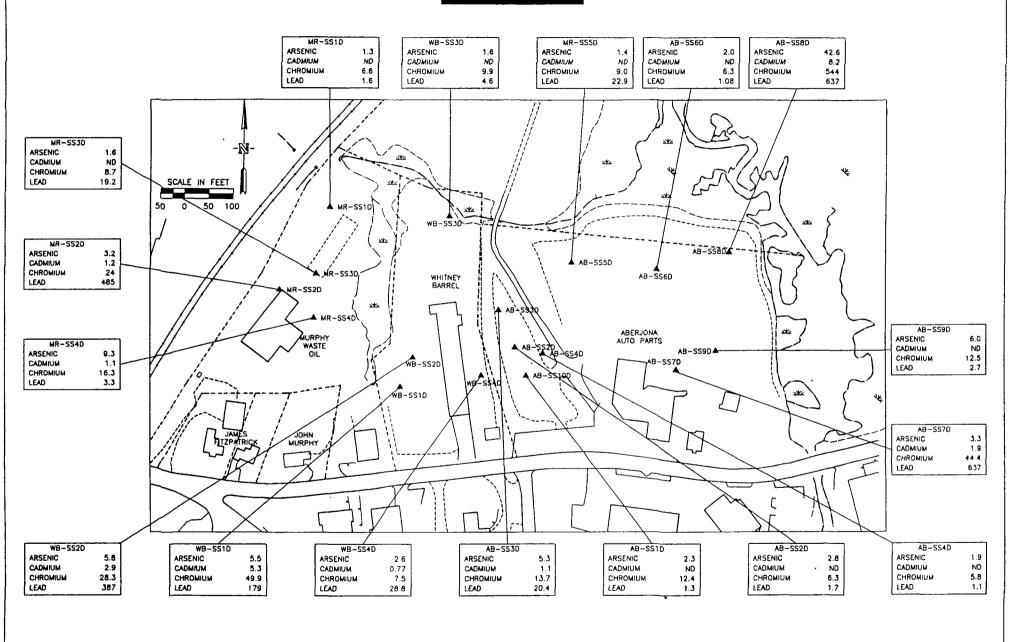


0681S003

SUBSURFACE SOIL PCB RESULTS
All Values are in mg/kg

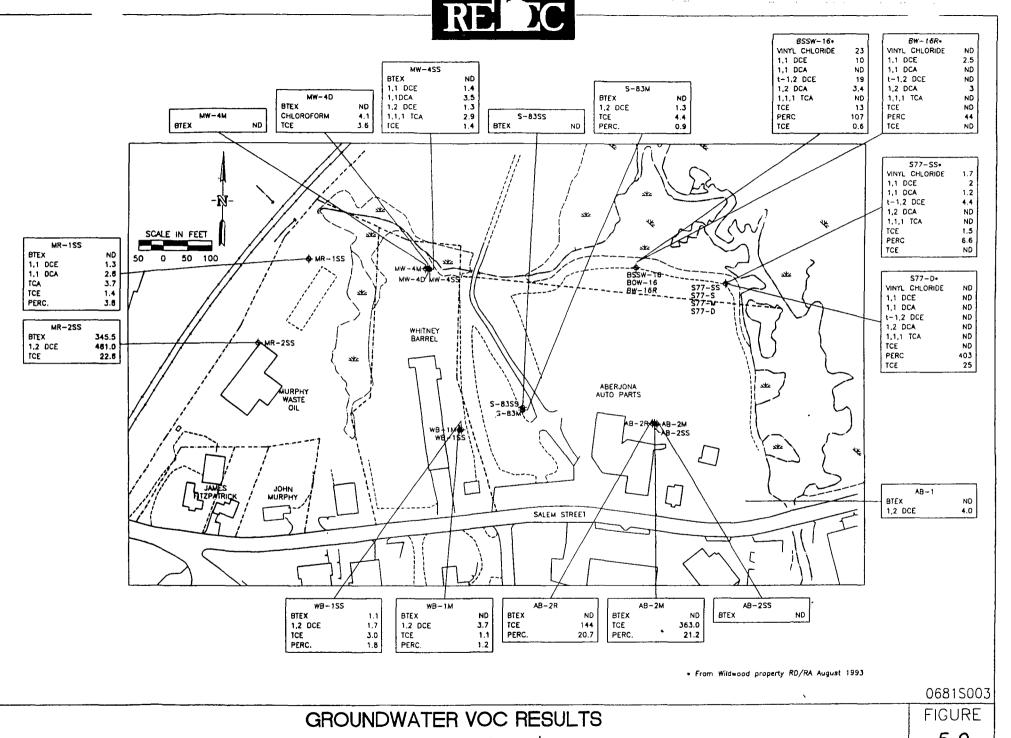
FIGURE **5-7** 

## REI DC



SUBSURFACE SOIL METALS RESULTS
All Values are in mg/kg

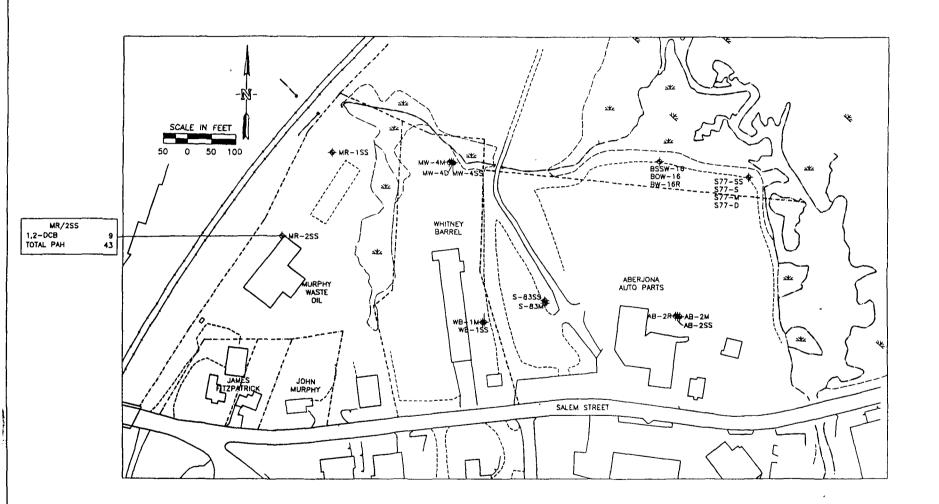
0681S003 FIGURE



All Values are in ug/L

5-9

# RE EC



• Pesticides not detected except as noted.

06815003

DETECTED GROUNDWATER SVOC AND PESITICIDE RESULTS
All Values are in ug/L

FIGURE

5-10

AP?. B



Commonwealth of Massachusetts

Executive Office of Environmental Affairs

## Department of Environmental Protection

William F. Weld
Governor
Trudy Coxe
Secretary, ECEA
Thomas B. Powers
Acting Commissioner

August 29, 1994

Certified Mail No. # P 328 155 920

Mr. Jules Selden, Esq.
Clean Harbors Environmental Services, Inc.
PO Box 9137
Quincy MA 02269-9137

Re: Approval Report Submittal Date Extension Request - M.G.L. c. 21C - Murphy's Waste Oil Service, Inc. MAD066588005

Dear: Mr. Selden

The Massachusetts Department of Environmental Protection, Bureau of Waste Prevention, Division of Hazardous Materials (hereinafter in this document referred to as the Department) has reviewed the following documents:

- Hydrogeologic Characterization Report, Murphy's Waste Oil Service, Inc. 252 Salem Street, Woburn, MA 01801, February 1, 1994 (Report); and
- Scope of Work for Subsurface Investigation. Murphy's Waste Oil Service, Inc. 252 Salem Street, Woburn, MA 01801, June 30, 1994 (Scope).

These documents were submitted to the Department on behalf of Murphy's Waste Oil Service, Inc. 252 Salem Street, Woburn, Massachusetts (Facility) by Clean Harbors Environmental Services, Inc. of Braintree Massachusetts in compliance with License Condition (10)(b) of the Facility's Part B Hazardous Waste Facility License.

The Department APPROVES the Report and Scope in accordance with Permit Condition (10)(i)(a) with the following modifications:

1. Any existing W89 series monitoring wells shown on Figure 6 of the Report shall be incorporated into the scope of work for purposes of groundwater elevation data and sampling. Such monitoring wells

MURPHSCOPE.APV August 29, 1994

> need not be sampled for the entire suite of parameters described on page 7, paragraph 2 of the Scope but shall be sampled for volatile organic compounds (EPA Method 8240). In addition, such monitoring wells shall be resurveyed for purposes of elevation control to the same datum as the proposed new monitoring wells; and redeveloped prior to sampling.

- 2. The Facility shall either install an additional shallow monitoring well in the eastern portion of the facility in the area of monitoring well W89-S16 or may utilize either monitoring well W89-S16 or W89-S3 in lieu of such a monitoring well. The monitoring well shall be sampled for the parameters listed on page 7, paragraph 2 of the Scope.
- 3. Proposed monitoring well MW-4 shall be relocated off the vehicular travel area to a location northeast of that shown in Figure 2 of the Scope in the area east of the dike wall adjacent to the fence.
- 4. The Facility shall avoid using road boxes to the maximum extent possible by relocating monitoring wells to the edge or outside of vehicular traffic areas. Monitoring wells shall be constructed with outer steel protective casings extending above the ground surface with concrete surface Monitoring wells installed adjacent to vehicular travel areas shall also be protected by protective bumpers.
- 5. Page 5, paragraphs two through four of the Scope describe the procedures and criteria for selection of soil samples. In addition to the soil samples proposed in the Scope:
  - a. Surface soil samples shall be collected from the 0 to 2 foot interval in each monitoring well boring except at monitoring well couplet locations. A surface (0-2 foot) soil sample need be collected from only one boring at locations where monitoring well couplets are to be installed (eg. MW-5 S&D). At locations where the monitoring wells are to be installed either through pavement or graveled areas the surface sample shall be collected from beneath the base of gravel or pavement to 2 feet;

### MURPHSCOPE.APV August 29, 1994

- b. An additional at depth soil sample shall be collected in the natural deposits beneath the fill per borehole (or monitoring well couplet) from the highest head space screened sample. If the head space screen samples in the natural soils are non-detect the soil sample shall be collected from the lowest 2-foot interval immediately above the water table. If stained soils are encountered beneath the fill a soil sample from the stained depth shall be collected in lieu of the above; and
- c. Total Petroleum Hydrocarbon analysis (TPH) shall be performed using the GC/FID methodology, as described in the Department's Policy # WSC-401-91, rather than the proposed IR method.
- 6. Page 6, paragraph three of the Scope describes the procedures and locations for collection of wetland sediment samples. The proposed wetland sampling shall be modified to reflect the following:
  - a. Sampling station SW-2 shall be relocated within the wetland approximately 60-70 feet northwest of the proposed location shown on Figure 2 of the Scope; and
  - b. An additional wetland sediment sample shall be collected at a location approximately midway between SW-2 and SW-3.
- 7. All activities shall be conducted in a manner consistent with the following Department policies:
  - DEP Policy #WSC-310-91 <u>Standard References for Monitoring Wells</u> April 1991; and
  - DEP Policy #WSC-401-91 <u>Policy for the Investigation</u>, Assessment, and Remediation of <u>Petroleum Releases Interim Site Investigation</u> <u>Protocol Document April 1991.</u>
- 8. All activities conducted at the Facility under this approval shall comply with the requirements of 310 CMR 40.0113 RCRA Authorized State Hazardous Waste Program (M.G.L.c. 21C and 310 CMR 30.000), as applicable.

MURPHSCOPE.APV August 29, 1994

License Condition 10(1)(a) allows the Department to approve the Report and Scope with modifications with the Facility's concurrence. If the Facility does not concur (accept) the modifications than the Scope shall be considered Disapproved by the Department pursuant to License Condition 10(i)(b) and the Facility shall submitted a new or modified Scope in compliance with License Condition 10(i)(c).

Should you have any questions regarding this matter please contact Mr. John A. Carrigan of my staff at (617) 292 - 5584.

Sincerely,

Mr. Al Nardone, EEVI

Hazardous Waste Program

AN/JAC/RF/jac

Attachment

CC: Health Agent City Hall Woburn, MA

> Dick Chalpin DEP/BWSC NERO Woburn, MA

> Ed Pawlowski DEP/BWP-DHM NERO Woburn, MA

Ana Stern DEP/BWP-DHM Boston, MA

Anna Mayor DEP/BWSC Boston, MA APP. C



spill, interrediately call the National Response Counter (800) 424-8802

case of emergency or

\_

### DEPARTMENT OF ENVIRONME [74] 94.

DIVISION OF HAZARDOUS WASTE

One Winter Street Boston, Massachusetti 02/105 (Form designed for use on elite (12-prtch) typewriter. Generator's US EPA ID No **UNIFORM HAZARDOUS** MAD066588005 WASTE MANIFEST aliyality Fe**der**s in Generator's Name and Mailing Address State Manifest Lagramen: Number н 696305 MA MURPHY'S WASTE OIL SERVICE INC 252 SALEM STREET 252-974 EM E. WOBURN, MA 01801 WOBURN, MA 02155 Generator's Phone ( 617-935-9066 State Trans. If CLEAN HARBORS ENV. SERVICES, INC. ให้คับ**ตั**รใจรื่อออก 6178491800 Transporter 2 Company Name US EPA ID Number Transporter's Phone: State Trans 15 MAD 039321250 HUNDUR ENV. 413298 esignated Facility Name and Site Address / CLEAN HARBORS OF BRAINTREE, INC Transporter's Phone 385 QUINCY AVE MAD053452637 G State Fecility's ID NOT REQUIRED BRAINTREE, MA 02184 Facility's Phone (617), 849-1807 H. Containers 13 US DOT Description (Including Proper Shipping Name, Hazard Class and ID Number) Totai Waste No MAGI OILY DEBRIS, NON D.O.T. REGULATED, NONE, N/A 002 DY 500 ic J. A (S) of 100 criple of the listed Above (include physical state and hazard code.) nating Codes for Wastes Listed Abov. CHE EMERGENCY CALL CHI AT 1-800-DIL-TANK IN CASE 1115 Special Handling Instructions and Additional Information 110 WO#: MU6693 11d 16 GENERATOR'S CERTIFICATION: I hereby declare that the contents of this consignment are fully and accurately described above o. ied, packed, marked, and labeled, and are in all respects in proper condition for transport by nichwa proper shapping name and are class according to applicable international and national government regulations. and that I have selected the practicable method of treatment, alorage, or disposal currently available to me which ment OR, if I am a small quantity generator, I have made a good faith effort to minimize my reste generation and mod that is available to me and that i can afford. Date Signatui Bønted/Tvoed Na nature Month 90 0 Receipt of Materials Day Month MALI YEA 3.5 A 20. Facility Owner or Operator. Certification of receipt of hazardous meterials covered by this manifest except as noted in Item 19. ž Date · Day Month Year

MAILS TO GENERATOR

will accept the waste the generator is shipping

APP. D

•

### CLEAN HARBORS ENVIRONMENTAL SERVICES, INC. QC Checked By: 325 Wood Road Boring No: MW-1 Braintree, MA 02184 (617 849-1800 Page: 1 of 1 Project Name: Murphy's Waste Oil Service. Inc. CHES Job #: EN-170 Project Location: Salem Street, Woburn, MA Field Book No. 93-029 Client Name: Same Well Elevation: 53.29 Boring Location: Northwest portion of site Driller: A. Caron CHES Personnel: S. Applebaum Drilling Contractor: Environmental Drilling, Inc. Start Date: Drilling Method: Hollow Stem Auger 10/13/94 Finish Date: Casing/Auger Size: 4 1/4" 10/13/94 Sampler: Split Spoon SAMPLE £ Headspace well screen FIELD CLASSIFICATION (2) Strata DEPTH Field (1) Notes Depth pen. rec. AND Type Change Blows per 6 (in) Screening (from - to) Depth **DRILLING INFORMATION** on split spoon Reading (ft) (in) No. 0 - 224/6 116-20-17-11 7 ppm Brown, dense, medium to fine SAND: little Silt; little medium to fine Gravel. Dry. Glass in sample. 2 - 4 11-13-12-16 SS-2 24/3 0.2 ppm Same. SS-3 4 - 6 24/13 15-17-14-16 3.6 ppm FILL Dense, coarse to fine SAND; some coarse 3 to fine Gravel; little Silt. Dry. 5 6' Brown, very dense, medium to fine (+) 24/11 SS-4 6 - 8 30-34-85-92 0.4 ppm SAND; and coarse to medium Gravel; little Silt. Wet. SS-5 8 - 9.2 24/12 65-82-100 5.4 ppm Tan, very dense, coarse to fine SAND; and coarse to fine Gravel; little Silt. SAND and GRAVEL 10 10/9 61-100 5.3 ppm SS-6 10 - 11 Same. 15 15 5 **Bottom of Boring PERCENTAGE** SAMPLE TYPES NOTES: BY WEIGHT = 35-50% SS - split spoon and (1) OVA { ppm = parts per million} = 20-35% ST - shelby tube some (2) The Burmister System is used for field classification of soils. = 10-20% AF - auger flight little (3) Color change from tan to black at 4'8". trace = 1-10% RC - rock core (4) Gravel is angular igneous and metamorphic rock; may be Till. (5) Set 2" PVC well at 15'. See Well Completion Report for **GRANULAR SOILS** COHESIVE SOILS details. N-value N-value Density Density very loose < 2 very soft 5 - 10 2 - 4 loose soft 11 - 30medium medium stiff 4 - 8 8 - 15 31 - 50 stiff dense <u>15</u> - 30 very stiff >50 very dense

#### CLEAN HARBORS ENVIRONMENTAL SERVICES, INC. QC Checked By: 325 Wood Road Boring No: MW-2 Braintree, MA 02184 Page: 1 of 1 (617 849-1800 Project Name: Murphy's Waste Oil Service. Inc. CHES Job #: EN-170 Project Location: Salem Street, Woburn, MA Field Book No. 93-029 Client Name: Same Well Elevation: 53.77' Boring Location: Southwest Comer Of Site Driller: A. Caron CHES Personnel: S Applebaum **Drilling Contractor:** Environmental Drilling, Inc. Start Date: Drilling Method: Hollow Stem Auger 10/12/94 Sampler: Split Spoon Finish Date: Casing/Auger Size: 4 1/4" 10/12/94 **SAMPLE** € Headspace screen (2) FIELD CLASSIFICATION DEPTH ( Strata Field (1) Notes Depth pen. AND Type Change Blows per 6 (in) Screening (from - to) rec. 8 DRILLING INFORMATION ₩ Depth on split spoon Reading (ft) (in) No. 0 - 2 SS-1 24/16 8-21-36-100 Brown and dark gray, very dense coarse 700 ppm to fine SAND; some Silt, little coarse to fine Gravel. Dry. SS-2 2 - 4 24/18 22-18-12-12 >1,000 ppm Dark gray, medium dense coarse to fine SAND; some Silt; little coarse to fine Gravel. Dry. Brown-gray, dense, ∞arse to fine SAND; 24/11 6-16-30-46 **SS-3** 4 - 6 FILL 720 ppm some Silt; little coarse to fine Gravel; little Clay. Moist. Some roots in tip of 5 spoon. SS-4 6 - 6.6 6/6 120 Spoon empty. 7.5' Brown-gray, dense, coarse to fine SAND; SS-4A 7.5 - 9.5 24/15 8-17-17-15 260 ppm and coarse to fine Gravel; trace Silt. 10 SS-5 10 - 12 24/10 20-18-20-18 220 ppm SAND Same. AND **GRAVEL** Brown, dense, coarse to fine SAND; little <u>12 -</u> 14 24/16 SS-6 14-18-20-18 185 ppm medium to fine Gravel; trace Silt. Brown, medium dense, coarse to fine SS-7 14 - 16 24/15 12-14-9-13 SAND; little medium to fine Gravel; trace 15' Silt. 15 3 **Bottom of Boring PERCENTAGE** SAMPLE TYPES NOTES: BY WEIGHT SS - split spoon and = 35-50% (1) OVA { ppm = parts per million} = 20-35% ST - shelby tube some (2) The Burmister System is used for field classification of soils. little = 10-20% (3) Set 2" PVC well at 15'. See Well Completion Report for AF - auger flight RC - rock core trace = 1-10%details. **GRANULAR SOILS COHESIVE SOILS** N-value Density N-value Density < 4 very loose < 2 very soft 5 - 10 2 - 4 soft loose 4 - 8 8 - 15 11 - 30 medium stiff medium 31 - 50stiff dense > 50 very dense 15 - 30 very stiff

	С	LEAN HARB	325	/IRONMENTAL SEF 5 Wood Road ree, MA 02184	RVICES, INC	•	QC Checked By: Boring No: MW-3		_		
	aia at ti	0.000	(6	17 849-1800			Page: 1 of 1		_		$\dashv$
Pr	oject N	ame: Murph	ny's Waste	e Oil Service, Inc.	<del> </del>		CHES Job #: EN-170 Field Book No. 93-029		—		
Cii	ent Na	me: Same	uem Stree	L WODUM MA	7		Well Elevation: 52,87'				
Во	ring Lo	cation: No	rthern por	tion of site			Driller: A. Caron		_		
				ental Drilling, Inc.			CHES Personnel: S. Appl	ebaı	ım		
		ethod: Holk		Auger			Start Date: 10/18/94				
	sing/Au	ıger Size: 4		Samp	ler: Split Sp	ľ	Finish Date: 10/18/94		<b>—</b>	_	
DEPTH (ft)	Туре	S. Depth	pen.	Plana as C (is)	Headspace Field (1)	Strata Change	FIELD CLASSIFICATION (2) AND	Notes	3	well screen	Strata
	& No.	(from - to) (ft)	rec. (in)	Blows per 6 (in) on split spoon	Screening Reading	Depth	DRILLING INFORMATION	Ž	•	Wells	ξ
	SS-1	0 - 2	24/16	12-15-13-12	2.0 ppm		Tan, medium dense, coarse to fine SAND some Silt; some coarse to medium Gravel Dry.				
	SS-2	2-4	24/15	12-10-10-8	2.2 ppm		Tan/brown, medium dense, coarse to medium SAND; trace Silt; trace Gravel. Dry.				
5	SS-3	4-6	24/0	16-18-16-20		FILL					
	SS-4	6 - 8	24/16	24-36-14-18	26 ppm	7.5'	Tan, dense, coarse to fine SAND; trace Silt. Peat in tip.				
	SS-5	8 - 10	24/21	28-44-43-47	100 ppm	<b>★</b> 8'	Brown, very dense medium SAND; trace Silt.	1	3		4
10	SS-6	10 - 12	24/24	8-14-25-33	460 ppm	SAND	Same.		3		
	SS-7	12 - 14	24/24	16-29-41-33	140 ppm		Tan, very dense, medium SAND; trace Silt.		3 1		
			1		ł	14'		ı		目	
15							Bottom of boring	1	4		
SAMPLE TYPES  SS - split spoon ST - shelby tube AF - auger flight RC - rock core  GRANULAR SOILS  PERCENTAGE BY WEIGHT and = 35-50% some = 20-35% little = 10-20% trace = 1-10%  COHESIVE SOILS					NOTES:  (1) OVA {ppm = parts per million}  (2) The Burmister System is used for field classification of soils.  (3) Hydrogen Sulfide odor in sample.  (4) Set 2" PVC well at 14'. See Well Completion Report for details.						
5 11 31	- 10 - 30 - 50	Density very loose loose medium dense ery dense 3490	2	2 very soft - 4 soft - 8 medium stiff 15 stiff							

### CLEAN HARBORS ENVIRONMENTAL SERVICES, INC. QC Checked By: 325 Wood Road Boring No: MW-4 Braintree, MA 02184 (617 849-1800 Page: 1 of 1 Project Name: Murphy's Waste Oil Service. Inc. CHES Job #: EN-170 Project Location: Salem Street, Woburn, MA Field Book No. 93-029 Client Name: Same Well Elevation: 52,23' Boring Location: Northeast portion of site Driller: A. Caron CHES Personnel: S Applebaum Drilling Contractor: Environmental Drilling, Inc. Start Date: Drilling Method: Hollow Stem Auger 10/12/94 Finish Date: Casing/Auger Size: 4 1/4" Sampler: Split Spoon 10/12/94 SAMPLE Headspace well screen (2)FIELD CLASSIFICATION EPTH ( Strata Field (1) pen. rec. Notes Strata Depth AND Type Change Blows per 6 (in) Screening (from - to) Depth **DRILLING INFORMATION** on split spoon Reading (ft) No. (in) 0 - 2 24/22 19-24-30-26 SS-1 0.2 ppm Dark brown/gray, very dense, medium to fine SAND; some coarse to 2 - 4 SS-2 24/15 75-35-36-34 ND Dark brown, very dense coarse to fine SAND; some coarse to fine Gravel; some Silt; trace Clay. Dry. Roots in sample. Dark brown, very dense coarse to fine 24/9 4 - 6 29-23-13-7 2.2 ppm FILL SAND; some coarse to fine Gravel; some Silt; trace Clay. Dry. 5 6' 3 24/17 Dark brown, dense coarse to fine SAND; SS-4 6 - 8 10-18-21-28 28 ppm some coarse to fine Gravel; little Silt. 8' 8 - 10 <u>SS-5</u> 24/18 8-18-22-25 46 ppm Light brown, dense medium to fine SAND; 4 trace Silt. 10 SS-6 10 - 12 24/24 13-22-29-36 Light brown, very dense medium to fine(+) 92 ppm SAND SAND; trace Gravel; trace Silt. AND GRAVEL 24/24 12 - 14 11-19-23-29 53 ppm Light brown, dense coarse to fine(+) SAND; trace medium to fine Gravel; trace 15' 15 5 **Bottom of Boring PERCENTAGE** SAMPLE TYPES NOTES: BY WEIGHT = 35-50% SS - split spoon and (1) OVA { ppm = parts per million} = 20-35% ST - shelby tube some (2) The Burmister System is used for field classification of soils. AF - auger flight = 10-20%little (3) Color change from dark to light brown at 7'. H2S odor in sample. RC - rock core trace = 1-10% (4) H<sub>2</sub>S odor in sample. (5) Set 2" PVC well at 15'. See Well Completion Report for **GRANULAR SOILS COHESIVE SOILS** details. N-value Density N-value Density < 4 very loose very soft < 2 5 - 10 2 - 4 loose soft 11 - 30 medium 4 - 8 8 - 15 medium stiff 31 - 50 stiff dense > 50 very dense 15 - 30very stiff Disk Name: 3490

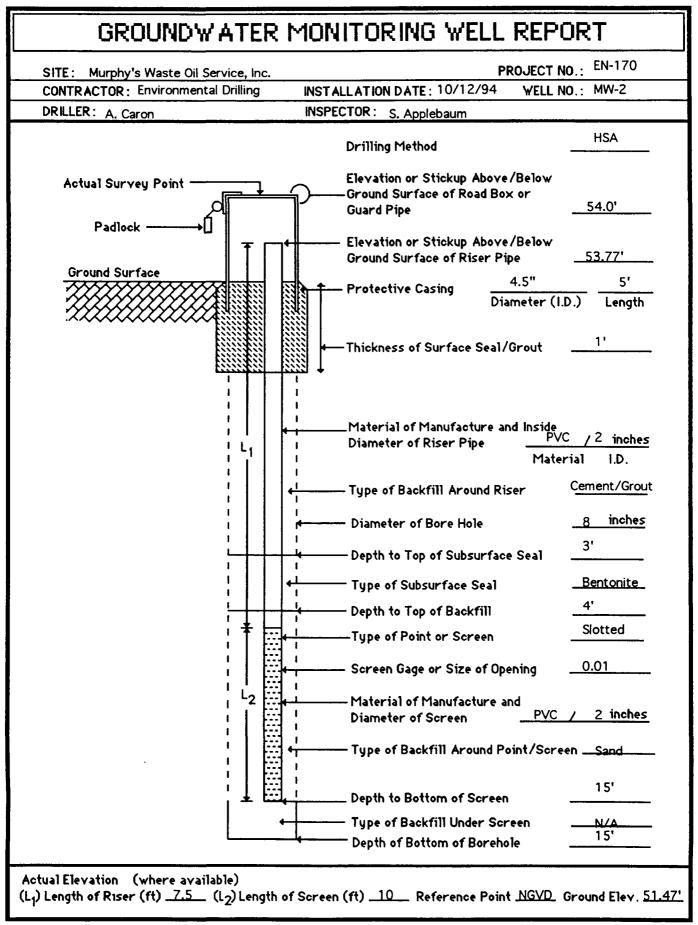
### **CLEAN HARBORS ENVIRONMENTAL SERVICES, INC.** QC Checked By: 325 Wood Road Boring No: MW-5S Braintree, MA 02184 (617.849-1800 Page: 1 of 1 Project Name: Murphy's Waste Oil Service, Inc. CHES Job #: EN-170 Project Location: Salem Street, Woburn, MA Field Book No. 93-029 Client Name: Same Well Elevation: 53.97' Boring Location: Eastern cortion of site Driller: A. Caron CHES Personnel: S. Applebaum Drilling Contractor: Environmental Drilling, Inc. Start Date: Drilling Method: Hollow Stem Auger 10/12/94 Finish Date: 10/12/94 Casing/Auger Size: 4 1/4" Sampler: Split Spoon SAMPLE € Headspace screen FIELD CLASSIFICATION (2)DEPTH ( Strata Field (1) pen. Notes Strata Depth Change AND Type Blows per 6 (in) Screening (from - to) 8 Depth DRILLING INFORMATION ¥e on split spoon Reading (ft) (in) No. SS-1 0-2 24/15 23-19-27-36 ND Brown/gray, dense, coarse to fine SAND; some coarse to fine Gravel; trace Silt. Brick in sample. Dry. SS-2 2 - 4 35-67-46-64 24/20 Brown, very dense, coarse to fine SAND; 0.4 ppm and coarse to fine Gravel; trace Silt. Drv. 24/16 SS-3 4 - 6 24-40-30-53 ND FILL Brown, very dense, (+) coarse to fine SAND; some ∞arse to fine Gravel; 5 trace Silt. Dry. Brown, very dense (+) coarse to fine 6 - 8 24/12 69-59-65-39 SS-4 SAND; and coarse to fine Gravel; trace 0.4 ppm Silt. Wet at tip. 8' Brown, dense, coarse to fine SAND; SS-5 24/9 8 - 10 24-25-25-20 1.2 ppm some medium to fine Gravel; trace Silt. 10' 10 24/17 6-9-11-13 SS-6 2.3 ppm 10 - 12 SAND Brown, medium dense, coarse to fine SAND; little coarse to fine Gravel, trace Silt SS-7 12 - 14 24/24 13-12-13-14 2.4 ppm Same. 15' 3 15 **Bottom of Boring PERCENTAGE** SAMPLE TYPES NOTES: BY WEIGHT SS - split spoon and = 35-50% (1) OVA { ppm = parts per million} = 20-35% (2) The Burmister System is used for field classification of soils. ST - shelby tube some AF - auger flight little = 10-20% (3) Set 2" PVC well at 15', See Well Completion Report for RC - rock core = 1-10% trace details. **GRANULAR SOILS COHESIVE SOILS** N-value Density N-value Density < 2 2 - 4 very loose very soft 5 - 10 soft loose medium stiff 11 - 30 medium 4 - 8 8 - 15 31 - 50 stiff dense > 50 very dense 15 - 30 very stiff

	C	LEAN HARB	325 Brainti	IRONMENTAL SER Wood Road ree, MA 02184	RVICES, INC.			QC Checked By: Boring No: MW-5D				
<u> </u>	ainat N	amar 14		7 849-1800				Page: 1 of 2 CHES Job #: EN-170			$\dashv$	
D <sub>m</sub>	oject I c	ocation: Se	ivs waste	Oil Service, Inc. t. Woburn, MA				Field Book No. 93-029				
Cli	ent Nar	ne: Same	nem Stree	t. Woburn. MA		•		Well Elevation: 53,79'				
		cation: Eas	stern porti	on of site	<del></del>			Driller: A. Caron				
				ental Drilling, Inc.	<del></del>			CHES Personnel: S. Apple	baun	n .		
		ethod: Holle						Start Date: 10/14/94				
		ıqer Size:			ler: Split Sp	oon		Finish Date: 10/18/94				
Œ		s	AMPLE	·	Headspace	l		(2)		ç		
DEPTH (ft)		Depth			Field (1)	Strata	FIELD CI	LASSIFICATION (2)	8	well screen	22	
<u> </u>	Type &	(from - to)	pen. rec.	Blows per 6 (in)	Screening	Change Depth	DOLL IN	AND G INFORMATION	Notes	န္တ	Strata	
8	No.	(ft)	(in)	on split spoon	Reading	Depui	DRILLIN	GINFORMATION	_	Į₹	ľ″l	
•		<del></del>	<del>- ` ´</del>						+	m		
	<b></b>			-	1	l	Į.		3	Ш		
					1	1				Ш		
					1					Ш		
	SS-1	19 - 21	24/8	38-33-26-30	4.2 ppm		Tan, very de	nse, coarse to fine SAND; to fine Gravel; trace Silt.		Ш		
20					1 pp	1	Some Coarse	to mie ciavei, trace cit.		Ш		
<b>I</b> .					1				ŀ	Ш		
					1	Į	Į.		Į.	Ш		
						İ	l			Ш		
1	SS-2	24 - 26	24/6	25-33-33-30	1.2 ppm			nse, coarse to fine SAND; o fine Gravel; little Silt.		Ш		
25					] ``		ano coarse t	o ilie Glavei, illie Siit.		Ш		
1						<b>!</b>	<b>,</b>			<b>\$</b>		
					1					Ш		
					4				1	Ш		
30 .	SS-3	29 - 31	24/5	24-24-34-26	2.6 ppm	SAND		nse, coarse to fine SAND;		Ш		
30			ļ		4	OAND	and coarse to	o fine Gravel; trace Silt.	l.	Ш		
			<del> </del>		4	i				Ш		
	<b> </b>				4	Ì				Ш		
•	00.4	01 00	04/0	00.40.40.07	-1					111		
35	SS-4	34 - 26	24/0	38-18-18-27	1		Coarse Gra	vel in tip.	1	Ш		
		<del></del>			4				1	Ш		
1 .					1	ŀ			l	Ш		
1					1		1		1	Ш		
	SS-5	39 - 41	24/15	19-24-32-27	6.2 ppm	1	Tan, very de	nse, medium to fine SAND;		Ш		
40	33-5	03 - 41	2-110	10 24 02 27	1 0.2 pp	]	some Silt.		1	Ш		
					1							
					]		1					
							l		1			
] ]	SS-6	44 - 46	24/6	24-25-30-25	3.3 ppm	1	Tan verv de	nse, coarse to fine SAND;	1			
45					7 ''			to fine Gravel, trace Silt.	1	Ш		
					]	Ţ	Į į	•	ı	Ш		
			4			<u> </u>	<u></u>		1_	Ш		
٩	AMPI F	TYPES		RCENTAGE	NOTES:							
1		lit spoon	and	BY WEIGHT I = 35-50%		000	rts per million				Ì	
		elby tube	son					r for field classification of soils	i_			
} 4	AF - aug	ger flight	little	= 10-20%	(3) 0 - 19	' characte	rized on boring	g log for MW-5S.	-			
		ck core	trac	×9 = 1-10%								
G	RANUL	AR SOILS	CO	HESIVE SOILS								
-	value	Density	N-va		1							
	< 4 \	ery loose		2 very soft	1							
	- 10	loose		- 4 soft	1							
	- 50	medium dense	84-	- 8 medium stiff 15 stiff								
		ery dense	15 -		<u> </u>			······································			لــــــــــــــــــــــــــــــــــــــ	

### CLEAN HARBORS ENVIRONMENTAL SERVICES, INC. QC Checked By: 325 Wood Road Boring No: MW-5D Braintree, MA 02184 (617 849-1800 Page: Project Name: Murphy's Waste Oil Service. Inc CHES Job #: EN-170 Project Location: Salem Street, Woburn, MA Field Book No. 93-029 Client Name: Same Well Elevation: 53.79' Boring Location: Eastern portion of site Driller: A. Caron CHES Personnel: S. Applebaum Drilling Contractor: Environmental Drilling. Inc. Start Date: Drilling Method: Hollow Stem Auger 10/14/94 Finish Date: Casing/Auger Size: 4 1/4" Sampler: Split Spoon 10/18/94 SAMPLE Headspace € well screen (2)FIELD CLASSIFICATION Strata DEPTH Field (1) Notes Strata Depth pen. **AND** Type Blows per 6 (in) Change Screening (from - to) Fec. 8 Depth **DRILLING INFORMATION** on split spoon Reading (ft) (in) No. **SS-7** 49 - 51 24/24 14-17-27-46 2.0 ppm Tan, dense, coarse to fine SAND; trace fine Gravel: trace Silt. SS-8 .54 - 56 24/17 35-24-32-52 Tan, very dense, coarse to fine SAND: 2.0 ppm SAND 55 some Silt; trace coarse Gravel. Dark tan/gray, dense, coarse to fine 24/22 14-22-22-41 SS-9 59 - 61 3.0 ppm SAND; little medium Gravel; trace 60 Silt. 63' Tan, dense, fine SAND; trace Silt. SS-10 64 - 66 24/15 8-13-20-32 0.6 ppm 65 **FINE** 69 - 71 24/16 14-16-17-17 SS-1 Gray, dense, very fine SAND. 0.8 ppm SAND 70 24/19 SS-12 74 - 76 14-23-22-30 1.6 ppm Same; trace Clay. 75 Gray, very dense, coarse to fine SAND; SS-13 79 - 81 24/18 21-24-31-32 0.3 ppm trace Silt; trace coarse Gravel. 80 83' Refusal PERCENTAGE SAMPLE TYPES NOTES: BY WEIGHT = 35-50% SS - split spoon and (1) OVA { ppm = parts per million} = 20-35% ST - shelby tube some (2) The Burmister System is used for field classification of soils. little = 10-20% AF - auger flight (3) 0 - 19' characterized on boring log for MW-5S. RC - rock core trace = 1-10% (4) Iron staining at 56'. (5) Set 2" PVC well at 83.5'. See Well Completion Report for **GRANULAR SOILS COHESIVE SOILS** details. N-value Density N-value Density < 4 very loose < 2 very soft 5 - 10 2 - 4 loose soft 11 - 30 medium stiff medium 4 - 8 8 - 15 31 - 50 stiff dense 15 - 30 very stiff > 50 very dense

### CLEAN HARBORS ENVIRONMENTAL SERVICES, INC. QC Checked By: 325 Wood Road Boring No: MW-6 Braintree, MA 02184 (617 849-1800 Page: 1 of 1 Project Name: Murphy's Waste Oil Service. Inc CHES Job #: EN-170 Project Location: Salem Street, Woburn, MA Field Book No. 93-029 Client Name: Same Well Elevation: 55.55' Boring Location: Southeast portion of site Driller: A. Caron CHES Personnel: S. Applebaum Drilling Contractor: Environmental Drilling, Inc. Start Date: Drilling Method: Hollow Stem Auger 10/13/94 Finish Date: 10/13/94 Casing/Auger Size: 4 1/4" Sampler: Split Spoon SAMPLE Headspace well screen FIELD CLASSIFICATION (2)DEPTH Strata Field (1) Strata Depth pen. AND Туре Change Blows per 6 (in) Screening (from - to) rec. Depth **DRILLING INFORMATION** on split spoon Reading No. (ft) (in) 24/17 0-2 14-18-20-14 SS-1 3.8 ppm Black, dense, medium to fine SAND: some coarse to fine Gravel; trace Brick. Dry. Brown, very dense, coarse to fine SAND; 2 - 4 24/20 69-74-85-79 SS-2 1.8 ppm some coarse to fine Gravel; little Silt. Dry. Tan, very dense, coarse to fine SAND; 4 - 6 24/16 25-31-30-40 mqq 8.0 some coarse to fine Gravel; trace Silt. Dry. 5 FILL 24/15 SS-4 6 - 8 31-41-38-41 0.7 ppm Same. Dry. Tan, very dense, coarse to fine SAND; **SS-5** 8 - 10 24/14 41-50-44-44 1.3 ppm some coarse to fine Gravel; trace Silt. Dry. 10' 10 Tan, very dense, (+) ∞arse to fine SAND; 24/12 23-26-23-17 3.5 ppm SS-6 10 - 12 and coarse to fine Gravel; little Silt. Wet. 12 - 14 19-22-28-31 Same. 24/4 4.7 ppm 12.5 SAND 15 GRAVEI Tan, dense, coarse to fine SAND; little medium to fine Gravel; trace Silt. SS-8 18 - 20 24/14 23-19-25-27 6.3 ppm **PERCENTAGE SAMPLE TYPES** NOTES: BY WEIGHT = 35-50% SS - split spoon and (1) OVA { ppm = parts per million} some = 20-35% ST - shelby tube (2) The Burmister System is used for field classification of soils. AF - auger flight little = 10-20% (3) Set 2" PVC well at 20'. See Well Completion Report for = 1-10% trace RC - rock core details. **GRANULAR SOILS COHESIVE SOILS** N-value Density N-value Density < 4 very loose < 2 very soft 5 - 10 2 - 4 loose soft 11 - 30 4 - 8 8 - 15 medium stiff medium 31 - 50 stiff dense > 50 very dense 15 - 30 very stiff

### GROUNDWATER MONITORING WELL REPORT PROJECT NO.: EN-170 SITE: Murphy's Waste Oil Service, Inc. CONTRACTOR: Environmental Drilling INSTALLATION DATE: 10/13/94 WELL NO .: MW-1 DRILLER: A. Caron INSPECTOR: S. Applebaum **HSA Drilling Method** Elevation or Stickup Above/Below Actual Survey Point -Ground Surface of Road Box or 53.43' Guard Pipe Padlock -Elevation or Stickup Above/Below Ground Surface of Riser Pipe 53.291 **Ground Surface Protective Casing** Diameter (I.D.) Length Thickness of Surface Seal/Grout .Material of Manufacture and Inside PVC /2 inches Diameter of Riser Pipe Material I.D. Cement/Grout Type of Backfill Around Riser inches - Diameter of Bore Hole 3' Depth to Top of Subsurface Seal Bentonite Type of Subsurface Seal Depth to Top of Backfill Slotted -Type of Point or Screen 0.01 · Screen Gage or Size of Opening L<sub>2</sub> Material of Manufacture and 2 inches PVC Diameter of Screen Type of Backfill Around Point/Screen <u>Sand</u> 15' Depth to Bottom of Screen Type of Backfill Under Screen Depth of Bottom of Borehole Actual Elevation (where available) (L1) Length of Riser (ft) 7.5 (L2) Length of Screen (ft) 10 Reference Point NGVD Ground Elev. 50.75'



### GROUNDWATER MONITORING WELL REPORT PROJECT NO.: EN-170 SITE: Murphy's Waste Oil Service, Inc. INSTALLATION DATE: 10/18/94 **CONTRACTOR:** Environmental Drilling WELL NO .: MW-3 DRILLER: A. Caron INSPECTOR: S. Applebaum **HSA Drilling Method** Elevation or Stickup Above/Below Actual Survey Point Ground Surface of Road Box or 53.27' Guard Pipe Padlock -Elevation or Stickup Above/Below 52.871 Ground Surface of Riser Pipe **Ground Surface** 4.5" Protective Casing Diameter (I.D.) Length Thickness of Surface Seal/Grout .Material of Manufacture and Inside PVC /2 inches Diameter of Riser Pipe **Material** I.D. Cement/Grout - Type of Backfill Around Riser inches 8 - Diameter of Bore Hole 2' Depth to Top of Subsurface Seal Bentonite Type of Subsurface Seal 3.5' Depth to Top of Backfill Slotted -Type of Point or Screen 0.01 Screen Gage or Size of Opening Material of Manufacture and 2 inches **PVC** Diameter of Screen Type of Backfill Around Point/Screen \_\_Sand\_ Depth to Bottom of Screen 14' Type of Backfill Under Screen Depth of Bottom of Borehole Actual Elevation (where available) (L<sub>1</sub>) Length of Riser (ft) \_\_6\_ (L<sub>2</sub>) Length of Screen (ft) \_\_10\_\_ Reference Point NGVD\_ Ground Elev. 50.74'

### GROUNDWATER MONITORING WELL REPORT PROJECT NO.: EN-170 SITE: Murphy's Waste Oil Service, Inc. WELL NO .: MW-4 **CONTRACTOR:** Environmental Drilling INSTALLATION DATE: 10/12/94 INSPECTOR: S. Applebaum DRILLER: A. Caron **HSA Drilling Method** Elevation or Stickup Above/Below Actual Survey Point Ground Surface of Road Box or 52.58' Guard Pipe Padlock -Elevation or Stickup Above/Below 52.23' Ground Surface of Riser Pipe **Ground Surface** Protective Casing Diameter (I.D.) Length Thickness of Surface Seal/Grout Material of Manufacture and Inside PVC / 2 inches Diameter of Riser Pipe Material I.D. Cement/Grout - Type of Backfill Around Riser 8 inches - Diameter of Bore Hole - Depth to Top of Subsurface Seal Bentonite Type of Subsurface Seal - Depth to Top of Backfill Slotted Type of Point or Screen 0.01 Screen Gage or Size of Opening Material of Manufacture and **PVC** 2 inches Diameter of Screen - Type of Backfill Around Point/Screen <u>Sand</u> 15' Depth to Bottom of Screen Type of Backfill Under Screen N/Δ 15' Depth of Bottom of Borehole

Actual Elevation (where available)

(L<sub>1</sub>) Length of Riser (ft) \_\_7.5\_\_ (L<sub>2</sub>) Length of Screen (ft) \_\_10\_\_ Reference Point NGVD\_ Ground Elev. 49.99'

### GROUNDWATER MONITORING WELL REPORT PROJECT NO.: EN-170 SITE: Murphy's Waste Oil Service, Inc. WELL NO .: MW-5S **CONTRACTOR:** Environmental Drilling INSTALLATION DATE: 10/12/94 DRILLER: A. Caron INSPECTOR: S. Applebaum **HSA Drilling Method** Elevation or Stickup Above/Below Actual Survey Point -Ground Surface of Road Box or 54.13' Guard Pipe Padlock -Elevation or Stickup Above/Below 53.97' Ground Surface of Riser Pipe **Ground Surface Protective Casing** Diameter (I.D.) Length 1' Thickness of Surface Seal/Grout Material of Manufacture and Inside PVC / 2 inches Diameter of Riser Pipe Material I.D. Cement/Grout Type of Backfill Around Riser inches - Diameter of Bore Hole Depth to Top of Subsurface Seal Bentonite Type of Subsurface Seal Depth to Top of Backfill Slotted -Type of Point or Screen 0.01 Screen Gage or Size of Opening Material of Manufacture and **PVC** 2 inches Diameter of Screen Type of Backfill Around Point/Screen \_\_Sand\_ 15' Depth to Bottom of Screen Type of Backfill Under Screen N/A 15' Depth of Bottom of Borehole Actual Elevation (where available) (L<sub>1</sub>) Length of Riser (ft) \_\_7.5\_\_ (L<sub>2</sub>) Length of Screen (ft) \_\_10\_\_ Reference Point NGVD\_ Ground Elev. 51.77'

### GROUNDWATER MONITORING WELL REPORT PROJECT NO .: EN-170 SITE: Murphy's Waste Oil Service, Inc. **CONTRACTOR:** Environmental Drilling INSTALLATION DATE: 10/18/94 WELL NO .: MW-5D DRILLER: A. Caron INSPECTOR: S. Applebaum **HSA Drilling Method** Elevation or Stickup Above/Below Actual Survey Point Ground Surface of Road Box or 53.98' **Guard Pipe** Padlock · Elevation or Stickup Above/Below Ground Surface of Riser Pipe 53.79' **Ground Surface Protective Casing** Diameter (I.D.) Length 69' Thickness of Surface Seal/Grout Material of Manufacture and Inside PVC / 2 inches Diameter of Riser Pipe **Material** I.D. Cement/Grout Type of Backfill Around Riser inches 8 Diameter of Bore Hole 69' Depth to Top of Subsurface Seal Bentonite Type of Subsurface Seal 71' Depth to Top of Backfill Slotted -Type of Point or Screen 0.01 Screen Gage or Size of Opening Material of Manufacture and **PVC** 2 inches Diameter of Screen Type of Backfill Around Point/Screen \_\_Sand\_ 83.5' Depth to Bottom of Screen Type of Backfill Under Screen N/A 83.5' Depth of Bottom of Borehole Actual Elevation (where available) (L<sub>1</sub>) Length of Riser (ft) \_\_7.5\_\_ (L<sub>2</sub>) Length of Screen (ft) \_\_10\_\_ Reference Point \_NGVD\_ Ground Elev. 51.65'

### GROUNDWATER MONITORING WELL REPORT PROJECT NO.: EN-170 SITE: Murphy's Waste Oil Service, Inc. INSTALLATION DATE: 10/13/94 WELL NO .: MW-6 **CONTRACTOR:** Environmental Drilling INSPECTOR: S. Applebaum DRILLER: A. Caron **HSA Drilling Method** Elevation or Stickup Above/Below Actual Survey Point Ground Surface of Road Box or 55.82' Guard Pipe Padlock -Elevation or Stickup Above/Below 55.55' Ground Surface of Riser Pipe Ground Surface 4.5" 5' Protective Casing Diameter (I.D.) Length 69' Thickness of Surface Seal/Grout Material of Manufacture and Inside PVC /2 inches Diameter of Riser Pipe Material I.D. Cement/Grout Type of Backfill Around Riser inches 8 Diameter of Bore Hole Depth to Top of Subsurface Seal Bentonite Type of Subsurface Seal Depth to Top of Backfill Slotted Type of Point or Screen 0.01 Screen Gage or Size of Opening Material of Manufacture and **PVC** 2 inches Diameter of Screen Type of Backfill Around Point/Screen Sand 18' Depth to Bottom of Screen N/A Type of Backfill Under Screen 18' Depth of Bottom of Borehole Actual Elevation (where available) (L<sub>1</sub>) Length of Riser (ft) 10 (L<sub>2</sub>) Length of Screen (ft) 10 Reference Point NGVD Ground Elev. 53.73'

REMEDIATION TECHNOLOGIES, INC.

# WELL INSTALLATION LOG Monitoring Well MR-1SS

9 Pond Lane Concord, MA 01742 (508)371-1422

'-	CHIN	OLO	OIE	), I	NC.		Monitoring Wen Pile 188		ĺ	(3	00)311-1422		
PROJE	CT NO:	3-06	81-33	2	L		DRILLING CO.: SOIL EXPLORATION	MP ELE	V.: 50.01	V.: 50.01' (MSL) (TOP OF PVC)			
CLIEN							ORILLER: JIN CAMPBELL		DEPTH: 1				
LOCAT	10N: A	OBURI	V, MA				BORING ID: 6	SURF A	CE ELEV.:	48.60	(MSL)		
START	DATE	: 8/16	/93	TIM	E: 0800		CASING ID: NA	WATER	LEVEL D	URING (	DRILLING: 4.92'		
COMPL	ETION	DATE	: 8/16	/93 7	TINE: 102	20	METHOD: HSA	PVC S	TICK-UP:	1.41'			
WELL	OCAT	ION: M	URPHY	WAS	TE OIL		LOGGED BY: MICHAEL T. COON						
DEPTH (feet)	RECOVERY (X)	SAMPLE DEPTH	PIO HEADSPACE (ppm)		ГІТНОГОСҮ		DESCRIPTION				TRUCTION PROTECTIVE STEEL MELL MONUMENT N/ LOCKING COVER		
		Ï			V 0	V.	EILL		Ω	88	1		
	50	0-2	0	12 12 13 10	00000000		Ory light brown medium to fine SAND. Little medium to fine angular Gravel. Trace Silt.		2' SCH.		BENTONITE SEAL GROUT	-	
5-	1		1		N. 6.	N.  -	OUTUACU		1	1:15:1	*   "	-5	
	44	5-7	0	12 12 13 15			OUTWASH Saturated fine to medium blonde SAND.		010 SLOTTED PVC SCREEN FROM 3' to 13'		SAND FROM 2 ' to 13'		
10-	40	10-12	0	13 10 17 19	0.00	). a	Saturated fine to medium blonde SANO and fine angular GRAVEL.  Bottom of Boring 13'.	· · · · · · · · · · · · · · · · · · ·	00			-10  -  -	
15-					nee							T5	
-	ARKS:	·									<del></del>		
1													

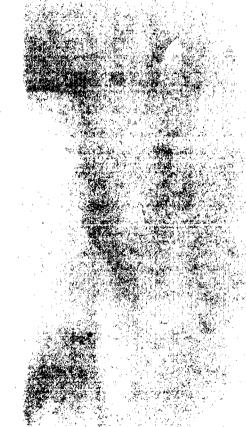
REMEDIATION TECHNOLOGIES, INC.

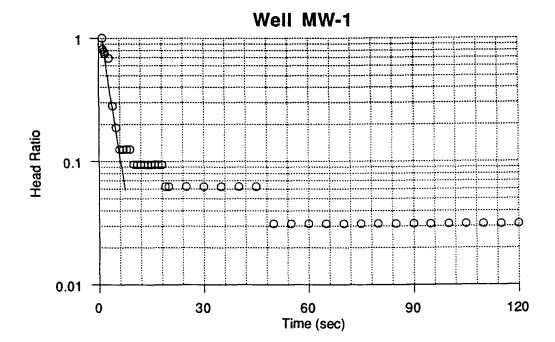
## WELL INSTALLATION LOG Monitoring Well MR-2SS

9 Pond Lane Concord, MA 01742 (508)371-1422

'-	O:		014	J, L				- 1			(00	0,57	1 1722	
PROJE	CT NO:	3-06	81-33	2	<del></del>	 DRILLING CO.: SOIL EXPLORATION	MF	ELE	V.: 50.37' (NSL) (TOP OF PVC)					$\neg \neg$
CLIEN	T: BEA	TRICE	-			DRILLER: JIN CAMPBELL			DEPTH:					
LOCAT						BORING ID: 6	St	JRFAC	E ELE	V.: 50.	30° (	MSL)	<del> </del>	
START					E: 0830	 CASING ID: NA			LEVEL			ILLIN	3: 5.91°	
					TINE: 1030	METHOD: HSA	P	C ST	ICK-UP	: 0.00	•			
WELL I	OCAT	ION: A	IURPHY	HAS	TE OIL	 LOGGED BY: MICHAEL T. COON								
DEPTH (feet)	RECOVERY (X)	SAMPLE DEPTH	PIO HEADSPACE (ppm)	BLOr' CTS. / 6"	LITHOLOGY	DESCRIPTION			WE	ELL CO			ON ,	
5-	45	0-2	0	19 23 20 18	000000000000000000000000000000000000000	EILL  Try light gray fine grained SAND and SILT  Ind angular medium GRAVEL.  Try dark brown fine SAND. Little Silt,  Trace subangular medium to fine Gravel.  Trace Clay.		٠٠٠	2° SCH, 40			GROUT FROM 0' to 2'	BENTONITE SEAL FROM 2' to 3'	<u></u>
10-	60,	5-7	-0	6 7 11 6		<u>OUTWASH</u> Saturated Dark brown CLAY and SAND. Trace subangular medium Gravel.			D PVC SCREEN			SAND SAND		10
	60	10-12	0.6	10 13 10 7		Saturated black to steel gray fine SAND a medium angular GRAVEL. Heavy petroleum odor. Saturated light brown medium SAND with counded medium Gravel. Petroleum odor.	and	اسمر.	0.010 SL01TED FROM 5'					
15-	44	15-17	0.2	11 15 15 20	0.000	Saturated well rounded fine to medium GRA. Little light brown Sand. Slight petroleum of Bottom of Boring 17°.						X	_	-15
20-	J	<u> </u>		1_										20_ا
REM	ARKS:											•		

# APP. E





L = 238 cm $T_0 = 1.6 \text{ sec}$   $K = 2.7 \times 10^{-2} \text{ cm/sec}$ 

### NOTES:

- 1. Rising head slug test performed by Clean Harbors on November 21, 1994.
- 2. Lis average length of screen through which water passed during the test.
- 3.  $T_0$  is time of recovery to 37 percent of initial change (h/h  $_0$ = 0.37), corrected for test start time.

İ	Α	PRELIMINARY				
	ISSUE	DESCRIPTION	DRWN	CHKD	APPR	DATE

# **CleanHarbo Environmental Services Companies**

325 WOOD ROAD BRAINTREE, MASSACHUSETTS 02184 (617) 849-1200

MURPHY'S WASTE OIL SERVICE, INC.

252 SALEM STREET WOBURN, MASSACHUSETTS

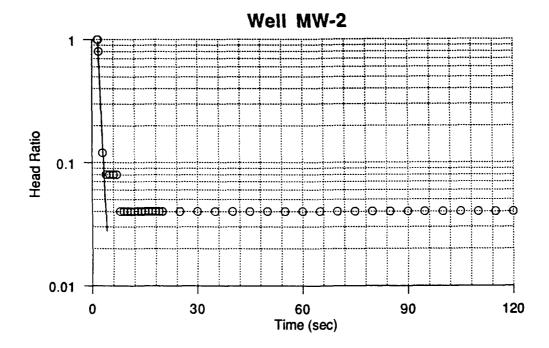
WELL MW-1 SLUG TEST

PROJECT NO. EN - 170

SCALE:

NA

DWG. NO.



L = 213 cm  $T_0 = 1.0 \text{ sec}$  $K = 4.6 \times 10^{-2} \text{ cm/sec}$ 

### NOTES:

- 1. Rising head slug test performed by Clean Harbors on November 21, 1994.
- 2. Lis average length of screen through which water passed during the test.
- 3. To is time of recovery to 37 percent of initial change (h/h = 0.37), corrected for test start time.

CleanHarbors
vironmental Services Companies

325 WOOD ROAD BRAINTREE, MASSACHUSETTS 02184 (617) 849-1200

Α	PRELIMINARY				
ISSUE	DESCRIPTION	DRWN	CHKD	APPR	DATE

### MURPHY'S WASTE OIL SERVICE, INC.

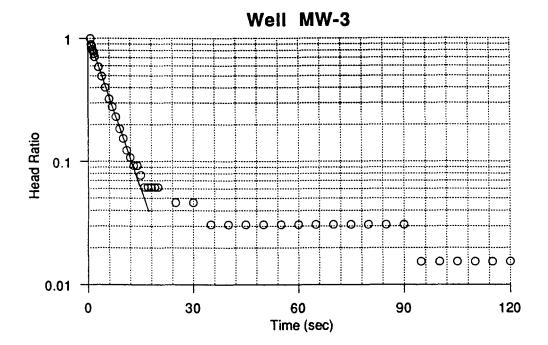
252 SALEM STREET WOBURN, MASSACHUSETTS

**WELL MW-2 SLUG TEST** 

PROJECT NO. EN - 170

SCALE: NA

DWG. NO.



L = 207 cm $T_0 = 4.6 \text{ sec}$   $K = 1.0 \times 10^{-2} \text{ cm/sec}$ 

### NOTES:

- 1. Rising head slug test performed by Clean Harbors on November 21, 1994.
- 2. Lis average length of screen through which water passed during the test.
- 3. To is time of recovery to 37 percent of initial change (h/h o= 0.37), corrected for test start time.



325 WOOD ROAD BRAINTREE, MASSACHUSETTS 02184 (617) 849-1200

Α	PRELIMINARY				
ISSUE	DESCRIPTION	DRWN	CHKD	APPR	DATE

## MURPHY'S WASTE OIL SERVICE, INC.

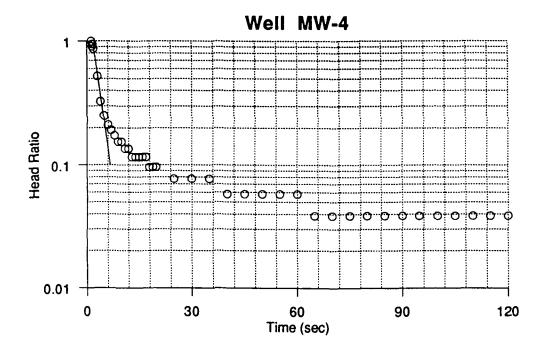
252 SALEM STREET WOBURN, MASSACHUSETTS

**WELL MW-3 SLUG TEST** 

PROJECT NO. EN - 170

DWG. NO.

SCALE:



L = 256 cm  $T_0$  = 2.4 sec K = 1.7 x 10<sup>-2</sup> cm/sec

### NOTES:

- 1. Rising head slug test performed by Clean Harbors on November 21, 1994.
- 2. L is average length of screen through which water passed during the test.
- 3. To is time of recovery to 37 percent of initial change (h/h = 0.37), corrected for test start time.

	ISSUE	DESCRIPTION	DRWN	CHKD	APPR	DATE
CleanHarbors	N	MURPHY'S WASTE OIL 252 SALEM STF WOBURN, MASSACH	REET		E, IN	C.

325 WOOD ROAD BRAINTREE, MASSACHUSETTS 02184 (617) 849-1200

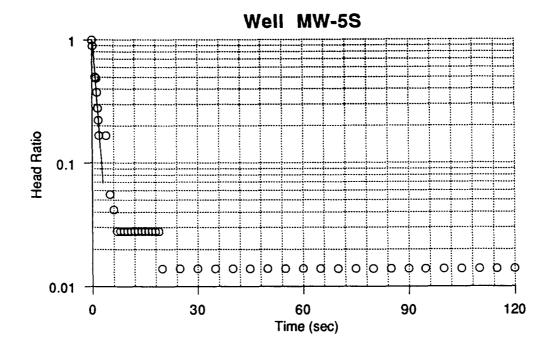
**Environmental Services Companies** 

PROJECT NO. EN - 170

DWG. NO.

WELL MW-4 SLUG TEST

SCALE: NA



$$L = 207 \text{ cm}$$
  
 $T_0 = 1.4 \text{ sec}$   
 $K = 3.4 \times 10^{-2} \text{ cm/sec}$ 

### NOTES:

- 1. Rising head slug test performed by Clean Harbors on November 21, 1994.
- 2. Lis average length of screen through which water passed during the test.
- 3. To is time of recovery to 37 percent of initial change (h/h = 0.37), corrected for test start time.

SCALE:

		FRELIMINANT				
	ISSUE	DESCRIPTION	DRWN	CHKD	APPR	DATE
	ML	JRPHY'S WASTE O	L SER	VICE	E, IN	C.
CleanHarbors	ŀ	252 SALEM S	TREET			

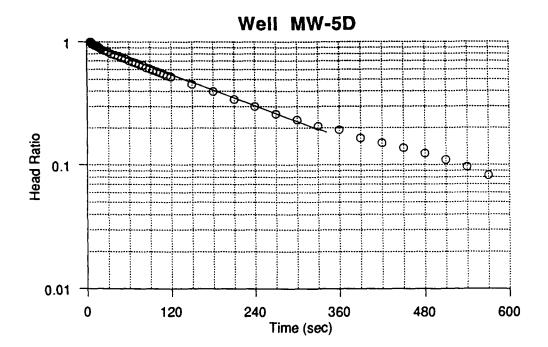
NA

# Environmental Services Companies

325 WOOD ROAD BRAINTREE, MASSACHUSETTS 02184 (617) 849-1200 WOBURN, MASSACHUSETTS
WELL MW-5S SLUG TEST

PROJECT NO. EN - 1	70 DWG	. NO.	

DOE! IMMINIADY



L = 305 cm  $T_0 = 190 \text{ sec}$  $K = 1.9 \times 10^{-4} \text{ cm/sec}$ 

### NOTES:

- 1. Rising head slug test performed by Clean Harbors on November 21, 1994.
- 2. Lis average length of screen through which water passed during the test.
- 3. To is time of recovery to 37 percent of initial change (h/h o= 0.37), corrected for test start time.

**Environmental Services Companies** 

325 WOOD ROAD BRAINTREE, MASSACHUSETTS 02184 (617) 849-1200

Α	PRELIMINARY				
ISSUE	DESCRIPTION	DRWN	CHKD	APPR	DATE

## MURPHY'S WASTE OIL SERVICE, INC.

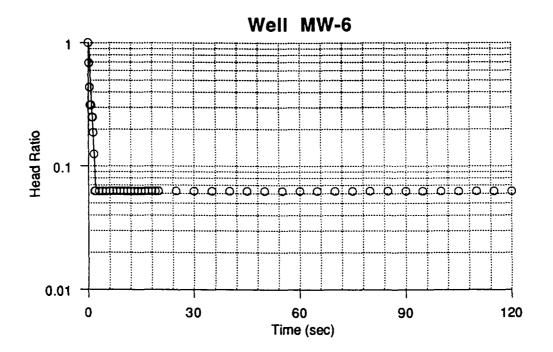
252 SALEM STREET WOBURN, MASSACHUSETTS

**WELL MW-5D SLUG TEST** 

PROJECT NO. EN - 170

SCALE: NA

DWG. NO.



L = 232 cm $T_0 = 0.5 \text{ sec}$   $K = 8.7 \times 10^{-2} \text{ cm/sec}$ 

### NOTES:

- 1. Rising head slug test performed by Clean Harbors on November 21, 1994.
- 2. Lis average length of screen through which water passed during the test.
- 3. To is time of recovery to 37 percent of initial change (h/h = 0.37), corrected for test start time.



**Environmental Services Companies** 

325 WOOD ROAD BRAINTREE, MASSACHUSETTS 02184 (617) 849-1200

Α	PRELIMINARY				
ISSUE	DESCRIPTION	DRWN	CHKD	APPR	DATE

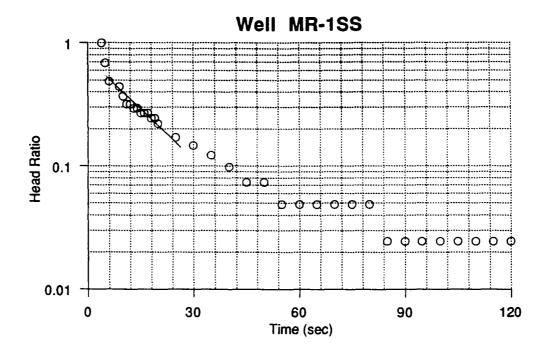
### MURPHY'S WASTE OIL SERVICE, INC.

252 SALEM STREET WOBURN, MASSACHUSETTS

**WELL MW-6 SLUG TEST** 

PROJECT NO. EN - 170

SCALE: NA DWG. NO.



L = 183 cm $T_0 = 5.9 \text{ sec}$   $K = 8.6 \times 10^{-3} \text{ cm/sec}$ 

### NOTES:

- 1. Rising head slug test performed by Clean Harbors on November 21, 1994.
- 2. L is average length of screen through which water passed during the test.
- 3.  $T_0$  is time of recovery to 37 percent of initial change (h/h  $_0$ = 0.37), corrected for test start time.

		ISSUE	DESCRIPTION	DRWN	CHKD	APPR	DATE		
ΔI - II	-	MURPHY'S WASTE OIL SERVICE, INC.							

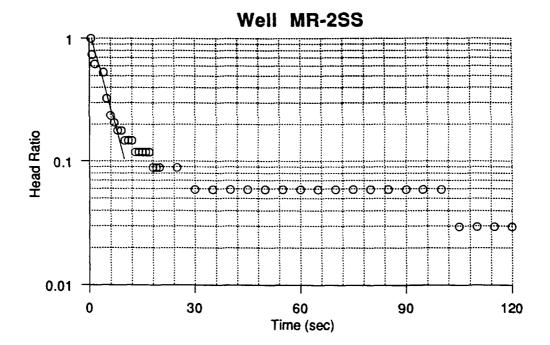
# TleanHarbors **Environmental Services Companies**

325 WOOD ROAD BRAINTREE, MASSACHUSETTS 02184 (617) 849-1200

WOBURN, MASSACHUSETTS WELL MR-1SS SLUG TEST

252 SALEM STREET

PROJECT NO. EN - 170 DWG. NO. SCALE: NA



$$L = 238 \text{ cm}$$
  
 $T_0 = 4.2 \text{ sec}$   
 $K = 1.0 \times 10^{-2} \text{ cm/sec}$ 

#### NOTES:

- 1. Rising head slug test performed by Clean Harbors on November 21, 1994.
- 2. Lis average length of screen through which water passed during the test.
- 3. To is time of recovery to 37 percent of initial change (h/h = 0.37), corrected for test start time.

	Α	PRELIMINARY				
_ !	ISSUE	DESCRIPTION	DRWN	CHKD	APPR	DATE

## CleanHarbors

**Environmental Services Companies** 

325 WOOD ROAD BRAINTREE, MASSACHUSETTS 02184 (617) 849-1200

#### MURPHY'S WASTE OIL SERVICE, INC.

252 SALEM STREET WOBURN, MASSACHUSETTS

**WELL MR-2SS SLUG TEST** 

PROJECT NO. EN - 170

SCALE: NA

DWG. NO.

## SLUG TEST DATA - WELL MW-1 Performed November 21, 1994

Time (min)	Time (sec)	Value (feet)	Elevation (feet)	Change (h)	Head Ratio (h/ho)
	(0007	(1001)		\***/	
0.0200	1.200	2.39	43.23	0.3200	1.0000
0.0233	1.398	2.45	43.29	0.2600	0.8125
0.0266	1.596	2.46	43.30	0.2500	0.7813
0.0300	1.800	2.47	43.31	0.2400	0.7500
0.0500	3.000	2.49	43.33	0.2200	0.6875
0.0666	3.996	2.62	43.46	0.0900	0.2813
0.0833	4.998	2.65	43.49	0.0600	0.1875
0.1000	6.000	2.67	43.51	0.0400	0.1250
0.1166	6.996	2.67	43.51	0.0400	0.1250
0.1333	7.998	2.67	43.51	0.0400	0.1250
0.1500	9.000	2.67	43.51	0.0400	0.1250
0.1666	9.996	2.68	43.52	0.0300	0.0937
0.1833	10.998	2.68	43.52	0.0300	0.0937
0.2000	12.000	2.68	43.52	0.0300	0.0937
0.2166	12.996	2.68	43.52	0.0300	0.0937
0.2333	13.998	2.68	43.52	0.0300	0.0937
0.2500	15.000	2.68	43.52	0.0300	0.0937
0.2666	15.996	2.68	43.52	0.0300	0.0937
0.2833	16.998	2.68	43.52	0.0300	0.0937
0.3000	18.000	2.68	43.52	0.0300	0.0937
0.3166	18.996	2.69	43.53	0.0200	0.0625
0.3333	19.998	2.69	43.53	0.0200	0.0625
0.4167	25.002	2.69	43.53	0.0200	0.0625
0.5000	30.000	2.69	43.53	0.0200	0.0625
0.5833	34.998	2.69	43.53	0.0200	0.0625
0.6667	40.002	2.69	43.53	0.0200	0.0625
0.7500	45.000	2.69	43.53	0.0200	0.0625
0.8333	49.998	2.70	43.54	0.0100	0.0312
0.9167	55.002	2.70	43.54	0.0100	0.0312
1.0000	60.000	2.70	43.54	0.0100	0.0312
1.0833	64.998	2.70	43.54	0.0100	0.0312
1.1667	70.002	2.70	43.54	0.0100	0.0312
1.2500	75.000	2.70	43.54	0.0100	0.0312
1.3330	79.980	2.70	43.54	0.0100	0.0312
1.4166	84.996	2.70	43.54	0.0100	0.0312
1.5000	90.000	2.70	43.54	0.0100	0.0312
1.5800	94.800	2.70	43.54	0.0100	0.0312
1.6667 -	100.002	2.70	43.54	0.0100	0.0312
1.7500	105.000	2.70	43.54	0.0100	0.0312
1.8333	109.998	2.70	43.54	0.0100	0.0312
1.9167	115.002	2.70	43.54	0.0100	0.0312
2.0000	120.000	2.70	43.54	0.0100	0.0312

## SLUG TEST DATA - WELL MW-2 Performed November 21, 1994

Time (min)	Time (sec)	Value (feet)	Elevation (feet)	Change (h)	Head Ratio (h/h <sub>0</sub> )
	(000)	(1007)	(14447		
0.0266	1.596	2.10	43.24	0.2500	1.0000
0.0300	1.800	2.10	43.24	0.2500	1.0000
0.0333	2.000	2.15	43.29	0.2000	0.8000
0.0500	3.000	2.32	43.46	0.0300	0.1200
0.0666	3.996	2.33	43.47	0.0200	0.0800
0.0833	4.998	2.33	43.47	0.0200	0.0800
0.1000	6.000	2.33	43.47	0.0200	0.0800
0.1166	6.996	2.33	43.47	0.0200	0.0800
0.1333	7.998	2.34	43.48	0.0100	0.0400
0.1500	9.000	2.34	43.48	0.0100	0.0400
0.1666	9.996	2.34	43.48	0.0100	0.0400
0.1833	10.998	2.34	43.48	0.0100	0.0400
0.2000	12.000	2.34	43.48	0.0100	0.0400
0.2166	12.996	2.34	43.48	0.0100	0.0400
0.2333	13.998	2.34	43.48	0.0100	0.0400
0.2500	15.000	2.34	43.48	0.0100	0.0400
0.2666	15.996	2.34	43.48	0.0100	0.0400
0.2833	16.998	2.34	43.48	0.0100	0.0400
0.3000	18.000	2.34	43.48	0.0100	0.0400
0.3166	18.996	2.34	43.48	0.0100	0.0400
0.3333	19.998	2.34	43.48	0.0100	0.0400
0.4167	25.002	2.34	43.48	0.0100	0.0400
0.5000	30.000	2.34	43.48	0.0100	0.0400
0.5833	34.998	2.34	43.48	0.0100	0.0400
0.6667	40.002	2.34	43.48	0.0100	0.0400
0.7500	45.000	2.34	43.48	0.0100	0.0400
0.8333	49.998	2.34	43.48	0.0100	0.0400
0.9167	55.002	2.34	43.48	0.0100	0.0400
1.0000	60.000	2.34	43.48	0.0100	0.0400
1.0833	64.998	2.34	43.48	0.0100	0.0400
1.1667	70.002	2.34	43.48	0.0100	0.0400
1.2500	75.000	2.34	43.48	0.0100	0.0400
1.3330	79.980	2.34	43.48	0.0100	0.0400
1.4166	84.996	2.34	43.48	0.0100	0.0400
1.5000	90.000	2.34	43.48	0.0100	0.0400
1.5800	94.800	2.34	43.48	0.0100	0.0400
1.6667	100.002	2.34	43.48	0.0100	0.0400
1.7500 -	105.000	2.34	43.48	0.0100	0.0400
1.8333	109.998	2.34	43.48	0.0100	0.0400
1.9167	115.002	2.34	43.48	0.0100	0.0400
2.0000	120.000	2.34	43.48	0.0100	0.0400

## SLUG TEST DATA - WELL MW-3 Performed November 21, 1994

Time (min)	Time (sec)	Value (feet)	Elevation (feet)	Change (h)	Head Ratio (h/h <sub>0</sub> )
		1.2.2.2.1	12447		1.407
0.0133	0.798	1.69	42.90	0.6500	1.0000
0.0166	0.996	1.76	42.97	0.5800	0.8923
0.0200	1.200	1.78	42.99	0.5600	0.8615
0.0233	1.398	1.81	43.02	0.5300	0.8154
0.0266	1.596	1.83	43.04	0.5100	0.7846
0.0300	1.800	1.85	43.06	0.4900	0.7538
0.0333	2.000	1.88	43.09	0.4600	0.7077
0.0500	3.000	1.96	43.17	0.3800	0.5846
0.0666	3.996	2.02	43.23	0.3200	0.4923
0.0833	4.998	2.08	43.29	0.2600	0.4000
0.1000	6.000	2.13	43.34	0.2100	0.3231
0.1166	6.996	2.16	43.37	0.1800	0.2769
0.1333	7.998	2.19	43.40	0.1500	0.2308
0.1500	9.000	2.22	43.43	0.1200	0.1846
0.1666	9.996	2.24	43.45	0.1000	0.1538
0.1833	10.998	2.26	43.47	0.0800	0.1231
0.2000	12.000	2.27	43.48	0.0700	0.1077
0.2166	12.996	2.28	43.49	0.0600	0.0923
0.2333	13.998	2.28	43.49	0.0600	0.0923
0.2500	15.000	2.29	43.50	0.0500	0.0769
0,2666	15.996	2.30	43.51	0.0400	0.0615
0.2833	16.998	2.30	43.51	0.0400	0.0615
0.3000	18.000	2.30	43.51	0.0400	0.0615
0.3166	18.996	2.30	43.51	0.0400	0.0615
0.3333	19.998	2.30	43.51	0.0400	0.0615
0.4167	25.002	2.31	43.52	0.0300	0.0462
0.5000	30.000	2.31	43.52	0.0300	0.0462
0.5833	34.998	2.32	43.53	0.0200	0.0308
0.6667	40.002	2.32	43.53	0.0200	0.0308
0.7500	45.000	2.32	43.53	0.0200	0.0308
0.8333	49.998	2.32	43.53	0.0200	0.0308
0.9167	55.002	2.32	43.53	0.0200	0.0308
1.0000	60.000	2.32	43.53	0.0200	0.0308
1.0833	64.998	2.32	43.53	0.0200	0.0308
1.1667	70.002	2.32	43.53	0.0200	0.0308
1.2500	75.000	2.32	43.53	0.0200	0.0308
1.3330	79.980	2.32	43.53	0.0200	0.0308
1.4166 -	84.996	2.32	43.53	0.0200	0.0308
1.5000	90.000	2.32	43.53	0.0200	0.0308
1.5800	94.800	2.33	43.54	0.0100	0.0154
1.6667	100.002	2.33	43.54	0.0100	0.0154
1.7500	105.000	2.33	43.54	0.0100	0.0154
1.8333	109.998	2.33	43.54	0.0100	0.0154
1.9167	115.002	2.33	43.54	0.0100	0.0154
2.0000	120.000	2.33	43.54	0.0100	0.0154
		55	73.37	0.0100	0.0127

## SLUG TEST DATA - WELL MW-4 Performed November 21, 1994

0.0233         1.398         2.62         42.84         0.5200         1.0000           0.0266         1.596         2.67         42.89         0.4700         0.9038           0.0300         1.800         2.65         42.87         0.4900         0.9423           0.0333         2.000         2.69         42.91         0.4500         0.8654           0.0500         3.000         2.87         43.09         0.2700         0.5192           0.0666         3.996         2.97         43.19         0.1700         0.3269           0.0833         4.998         3.01         43.23         0.1300         0.2500           0.1000         6.000         3.03         43.25         0.1100         0.2115           0.1166         6.996         3.04         43.26         0.1000         0.1923           0.1333         7.998         3.05         43.27         0.0900         0.1731           0.1500         9.000         3.06         43.28         0.0800         0.1538           0.1833         10.998         3.07         43.29         0.0700         0.1346           0.2000         12.000         3.07         43.29         0.0700         <	Time (min)	Time (sec)	Value (feet)	Elevation (feet)	Change (h)	Head Ratio (h/ho)
0.0266         1.596         2.67         42.89         0.4700         0.9038           0.0300         1.800         2.65         42.87         0.4900         0.9423           0.0333         2.000         2.69         42.91         0.4500         0.8654           0.0500         3.000         2.87         43.09         0.2700         0.5192           0.0666         3.996         2.97         43.19         0.1700         0.3269           0.0833         4.998         3.01         43.23         0.1300         0.2500           0.1000         6.000         3.03         43.25         0.1100         0.2115           0.1166         6.996         3.04         43.26         0.1000         0.1923           0.1333         7.998         3.05         43.27         0.0900         0.1731           0.1500         9.000         3.06         43.28         0.0800         0.1538           0.1666         9.996         3.06         43.28         0.0800         0.1538           0.1833         10.998         3.07         43.29         0.0700         0.1346           0.2166         12.996         3.08         43.30         0.0600         <						
0.0300         1.800         2.65         42.87         0.4900         0.9423           0.0333         2.000         2.69         42.91         0.4500         0.8654           0.0500         3.000         2.87         43.09         0.2700         0.5192           0.0666         3.996         2.97         43.19         0.1700         0.3269           0.0833         4.998         3.01         43.23         0.1300         0.2500           0.1000         6.000         3.03         43.25         0.1100         0.2115           0.1166         6.996         3.04         43.26         0.1000         0.1923           0.1333         7.998         3.05         43.27         0.0900         0.1731           0.1500         9.000         3.06         43.28         0.0800         0.1538           0.1666         9.996         3.06         43.28         0.0800         0.1538           0.1833         10.998         3.07         43.29         0.0700         0.1346           0.2000         12.000         3.07         43.29         0.0700         0.1346           0.2166         12.996         3.08         43.30         0.0600						
0.0333         2.000         2.69         42.91         0.4500         0.8654           0.0500         3.000         2.87         43.09         0.2700         0.5192           0.0666         3.996         2.97         43.19         0.1700         0.3269           0.0833         4.998         3.01         43.23         0.1300         0.2500           0.1000         6.000         3.03         43.25         0.1100         0.2115           0.1166         6.996         3.04         43.26         0.1000         0.1923           0.1333         7.998         3.05         43.27         0.0900         0.1731           0.1500         9.000         3.06         43.28         0.0800         0.1538           0.1666         9.996         3.06         43.28         0.0800         0.1538           0.1833         10.998         3.07         43.29         0.0700         0.1346           0.2000         12.000         3.07         43.29         0.0700         0.1346           0.2166         12.996         3.08         43.30         0.0600         0.1154           0.2500         15.000         3.08         43.30         0.0600						
0.0500       3.000       2.87       43.09       0.2700       0.5192         0.0666       3.996       2.97       43.19       0.1700       0.3269         0.0833       4.998       3.01       43.23       0.1300       0.2500         0.1000       6.000       3.03       43.25       0.1100       0.2115         0.1166       6.996       3.04       43.26       0.1000       0.1923         0.1333       7.998       3.05       43.27       0.0900       0.1731         0.1500       9.000       3.06       43.28       0.0800       0.1538         0.1666       9.996       3.06       43.28       0.0800       0.1538         0.1833       10.998       3.07       43.29       0.0700       0.1346         0.2000       12.000       3.07       43.29       0.0700       0.1346         0.2166       12.996       3.08       43.30       0.0600       0.1154         0.2333       13.998       3.08       43.30       0.0600       0.1154         0.2833       16.998       3.08       43.30       0.0600       0.1154         0.2833       16.998       3.08       43.31       0.0500						
0.0666       3.996       2.97       43.19       0.1700       0.3269         0.0833       4.998       3.01       43.23       0.1300       0.2500         0.1000       6.000       3.03       43.25       0.1100       0.2115         0.1166       6.996       3.04       43.26       0.1000       0.1923         0.1333       7.998       3.05       43.27       0.0900       0.1731         0.1500       9.000       3.06       43.28       0.0800       0.1538         0.1666       9.996       3.06       43.28       0.0800       0.1538         0.1833       10.998       3.07       43.29       0.0700       0.1346         0.2000       12.000       3.07       43.29       0.0700       0.1346         0.2166       12.996       3.08       43.30       0.0600       0.1154         0.2333       13.998       3.08       43.30       0.0600       0.1154         0.2833       16.998       3.08       43.30       0.0600       0.1154         0.2833       16.998       3.08       43.31       0.0500       0.0962         0.3166       18.996       3.09       43.31       0.0500						
0.0833       4.998       3.01       43.23       0.1300       0.2500         0.1000       6.000       3.03       43.25       0.1100       0.2115         0.1166       6.996       3.04       43.26       0.1000       0.1923         0.1333       7.998       3.05       43.27       0.0900       0.1731         0.1500       9.000       3.06       43.28       0.0800       0.1538         0.1666       9.996       3.06       43.28       0.0800       0.1538         0.1833       10.998       3.07       43.29       0.0700       0.1346         0.2000       12.000       3.07       43.29       0.0700       0.1346         0.2166       12.996       3.08       43.30       0.0600       0.1154         0.2333       13.998       3.08       43.30       0.0600       0.1154         0.2500       15.000       3.08       43.30       0.0600       0.1154         0.2833       16.998       3.08       43.30       0.0600       0.1154         0.3000       18.000       3.09       43.31       0.0500       0.0962         0.3166       18.996       3.09       43.31       0.0500						
0.1000       6.000       3.03       43.25       0.1100       0.2115         0.1166       6.996       3.04       43.26       0.1000       0.1923         0.1333       7.998       3.05       43.27       0.0900       0.1731         0.1500       9.000       3.06       43.28       0.0800       0.1538         0.1666       9.996       3.06       43.28       0.0800       0.1538         0.1833       10.998       3.07       43.29       0.0700       0.1346         0.2000       12.000       3.07       43.29       0.0700       0.1346         0.2166       12.996       3.08       43.30       0.0600       0.1154         0.2333       13.998       3.08       43.30       0.0600       0.1154         0.2500       15.000       3.08       43.30       0.0600       0.1154         0.2833       16.998       3.08       43.30       0.0600       0.1154         0.3000       18.000       3.09       43.31       0.0500       0.0962         0.3166       18.996       3.09       43.31       0.0500       0.0962         0.3333       19.998       3.09       43.31       0.0500						
0.1166       6.996       3.04       43.26       0.1000       0.1923         0.1333       7.998       3.05       43.27       0.0900       0.1731         0.1500       9.000       3.06       43.28       0.0800       0.1538         0.1666       9.996       3.06       43.28       0.0800       0.1538         0.1833       10.998       3.07       43.29       0.0700       0.1346         0.2000       12.000       3.07       43.29       0.0700       0.1346         0.2166       12.996       3.08       43.30       0.0600       0.1154         0.2333       13.998       3.08       43.30       0.0600       0.1154         0.2500       15.000       3.08       43.30       0.0600       0.1154         0.2833       16.998       3.08       43.30       0.0600       0.1154         0.3000       18.000       3.09       43.31       0.0500       0.0962         0.3166       18.996       3.09       43.31       0.0500       0.0962         0.3333       19.998       3.09       43.31       0.0500       0.0962						
0.1333       7.998       3.05       43.27       0.0900       0.1731         0.1500       9.000       3.06       43.28       0.0800       0.1538         0.1666       9.996       3.06       43.28       0.0800       0.1538         0.1833       10.998       3.07       43.29       0.0700       0.1346         0.2000       12.000       3.07       43.29       0.0700       0.1346         0.2166       12.996       3.08       43.30       0.0600       0.1154         0.2333       13.998       3.08       43.30       0.0600       0.1154         0.2500       15.000       3.08       43.30       0.0600       0.1154         0.2833       16.998       3.08       43.30       0.0600       0.1154         0.3000       18.000       3.09       43.31       0.0500       0.0962         0.3166       18.996       3.09       43.31       0.0500       0.0962         0.3333       19.998       3.09       43.31       0.0500       0.0962						
0.1500       9.000       3.06       43.28       0.0800       0.1538         0.1666       9.996       3.06       43.28       0.0800       0.1538         0.1833       10.998       3.07       43.29       0.0700       0.1346         0.2000       12.000       3.07       43.29       0.0700       0.1346         0.2166       12.996       3.08       43.30       0.0600       0.1154         0.2333       13.998       3.08       43.30       0.0600       0.1154         0.2500       15.000       3.08       43.30       0.0600       0.1154         0.2666       15.996       3.08       43.30       0.0600       0.1154         0.2833       16.998       3.08       43.30       0.0600       0.1154         0.3000       18.000       3.09       43.31       0.0500       0.0962         0.3166       18.996       3.09       43.31       0.0500       0.0962         0.3333       19.998       3.09       43.31       0.0500       0.0962						
0.1666       9.996       3.06       43.28       0.0800       0.1538         0.1833       10.998       3.07       43.29       0.0700       0.1346         0.2000       12.000       3.07       43.29       0.0700       0.1346         0.2166       12.996       3.08       43.30       0.0600       0.1154         0.2333       13.998       3.08       43.30       0.0600       0.1154         0.2500       15.000       3.08       43.30       0.0600       0.1154         0.2666       15.996       3.08       43.30       0.0600       0.1154         0.2833       16.998       3.08       43.30       0.0600       0.1154         0.3000       18.000       3.09       43.31       0.0500       0.0962         0.3166       18.996       3.09       43.31       0.0500       0.0962         0.3333       19.998       3.09       43.31       0.0500       0.0962						
0.1833       10.998       3.07       43.29       0.0700       0.1346         0.2000       12.000       3.07       43.29       0.0700       0.1346         0.2166       12.996       3.08       43.30       0.0600       0.1154         0.2333       13.998       3.08       43.30       0.0600       0.1154         0.2500       15.000       3.08       43.30       0.0600       0.1154         0.2666       15.996       3.08       43.30       0.0600       0.1154         0.2833       16.998       3.08       43.30       0.0600       0.1154         0.3000       18.000       3.09       43.31       0.0500       0.0962         0.3166       18.996       3.09       43.31       0.0500       0.0962         0.3333       19.998       3.09       43.31       0.0500       0.0962						
0.2000       12.000       3.07       43.29       0.0700       0.1346         0.2166       12.996       3.08       43.30       0.0600       0.1154         0.2333       13.998       3.08       43.30       0.0600       0.1154         0.2500       15.000       3.08       43.30       0.0600       0.1154         0.2666       15.996       3.08       43.30       0.0600       0.1154         0.2833       16.998       3.08       43.30       0.0600       0.1154         0.3000       18.000       3.09       43.31       0.0500       0.0962         0.3166       18.996       3.09       43.31       0.0500       0.0962         0.3333       19.998       3.09       43.31       0.0500       0.0962						
0.2166       12.996       3.08       43.30       0.0600       0.1154         0.2333       13.998       3.08       43.30       0.0600       0.1154         0.2500       15.000       3.08       43.30       0.0600       0.1154         0.2666       15.996       3.08       43.30       0.0600       0.1154         0.2833       16.998       3.08       43.30       0.0600       0.1154         0.3000       18.000       3.09       43.31       0.0500       0.0962         0.3166       18.996       3.09       43.31       0.0500       0.0962         0.3333       19.998       3.09       43.31       0.0500       0.0962						
0.2333       13.998       3.08       43.30       0.0600       0.1154         0.2500       15.000       3.08       43.30       0.0600       0.1154         0.2666       15.996       3.08       43.30       0.0600       0.1154         0.2833       16.998       3.08       43.30       0.0600       0.1154         0.3000       18.000       3.09       43.31       0.0500       0.0962         0.3166       18.996       3.09       43.31       0.0500       0.0962         0.3333       19.998       3.09       43.31       0.0500       0.0962						
0.2500       15.000       3.08       43.30       0.0600       0.1154         0.2666       15.996       3.08       43.30       0.0600       0.1154         0.2833       16.998       3.08       43.30       0.0600       0.1154         0.3000       18.000       3.09       43.31       0.0500       0.0962         0.3166       18.996       3.09       43.31       0.0500       0.0962         0.3333       19.998       3.09       43.31       0.0500       0.0962						
0.2666       15.996       3.08       43.30       0.0600       0.1154         0.2833       16.998       3.08       43.30       0.0600       0.1154         0.3000       18.000       3.09       43.31       0.0500       0.0962         0.3166       18.996       3.09       43.31       0.0500       0.0962         0.3333       19.998       3.09       43.31       0.0500       0.0962						
0.2833       16.998       3.08       43.30       0.0600       0.1154         0.3000       18.000       3.09       43.31       0.0500       0.0962         0.3166       18.996       3.09       43.31       0.0500       0.0962         0.3333       19.998       3.09       43.31       0.0500       0.0962						
0.3000       18.000       3.09       43.31       0.0500       0.0962         0.3166       18.996       3.09       43.31       0.0500       0.0962         0.3333       19.998       3.09       43.31       0.0500       0.0962						
0.3166     18.996     3.09     43.31     0.0500     0.0962       0.3333     19.998     3.09     43.31     0.0500     0.0962						
0.3333 19.998 3.09 43.31 0.0500 0.0962						
0.4167 25.002 3.10 43.32 0.0400 0.0769						
0.5000 30.000 3.10 43.32 0.0400 0.0769						
0.5833 34.998 3.10 43.32 0.0400 0.0769						
0.6667 40.002 3.11 43.33 0.0300 0.0577	0.6667	40.002	3.11	43.33	0.0300	0.0577
0.7500 45.000 3.11 43.33 0.0300 0.0577	0.7500	45.000	3.11	43.33	0.0300	0.0577
0.8333 49.998 3.11 43.33 0.0300 0.0577	0.8333	49.998	3.11	43.33	0.0300	0.0577
0.9167 55.002 3.11 43.33 0.0300 0.0577	0.9167	55.002	3.11	43.33	0.0300	0.0577
1.0000 60.000 3.11 43.33 0.0300 0.0577	1.0000	60.000	3.11	43.33	0.0300	0.0577
1.0833 64.998 3.12 43.34 0.0200 0.0385	1.0833	64.998	3.12	43.34	0.0200	0.0385
1.1667 70.002 3.12 43.34 0.0200 0.0385	1.1667	70.002	3.12		0.0200	0.0385
1.2500 75.000 3.12 43.34 0.0200 0.0385	1.2500	75.000	3.12	43.34	0.0200	0.0385
1.3330 79.980 3.12 43.34 0.0200 0.0385	1.3330	79.980	3.12	43.34	0.0200	0.0385
1.4166 84.996 3.12 43.34 0.0200 0.0385	1.4166	84.996	3.12	43.34	0.0200	0.0385
1.5000 90.000 3.12 43.34 0.0200 0.0385	1.5000	90.000	3.12	43.34	0.0200	0.0385
1.5800 94.800 3.12 43.34 0.0200 0.0385	1.5800	94.800	3.12	43.34	0.0200	0.0385
1.6667 100.002 3.12 43.34 0.0200 0.0385	1.6667	100.002		43.34		
1.7500 105.000 3.12 43.34 0.0200 0.0385	1.7500	105.000	3.12	43.34		
1.8333 109.998 3.12 43.34 0.0200 0.0385						
1.9167 115.002 3.12 43.34 0.0200 0.0385						
2.0000 120.000 3.12 43.34 0.0200 0.0385						

#### SLUG TEST DATA - WELL MW-5S Performed November 21, 1994

Time	Time	Value	Elevation	Change	Head Ratio
<u>(min)</u>	(sec)	(feet)	(feet)	<u>(h)</u>	(h/h <sub>O</sub> )
0.0000	0.000		40.04	0.5000	1 0000
0.0000	0.000	2.02	42.84	0.7200	1.0000
0.0033	0.198	2.10	42.92	0.6400	0.8889
0.0133	0.798	2.38	43.20	0.3600	0.5000
0.0200	1.200	2.39	43.21	0.3500	0.4861
0.0233	1.398	2.47	43.29	0.2700	0.3750
0.0266	1.596	2.54	43.36	0.2000	0.2778
0.0300	1.800	2.58	43.40	0.1600	0.2222
0.0333	2.000	2.62	43.44	0.1200	0.1667
0.0666	3.996	2.62	43.44	0.1200	0.1667
0.0833	4.998	2.70	43.52	0.0400	0.0556
0.1000	6.000	2.71	43.53	0.0300	0.0417
0.1166	6.996	2.72	43.54	0.0200	0.0278
0.1333	7.998	2.72	43.54	0.0200	0.0278
0.1500	9.000	2.72	43.54	0.0200	0.0278
0.1666	9.996	2.72	43.54	0.0200	0.0278
0.1833	10.998	2.72	43.54	0.0200	0.0278
0.2000	12.000	2.72	43.54	0.0200	0.0278
0.2166	12.996	2.72	43.54	0.0200	0.0278
0.2333	13.998	2.72	43.54	0.0200	0.0278
0.2500	15.000	2.72	43.54	0.0200	0.0278
0.2666	15.996	2.72	43.54	0.0200	0.0278
0.2833	16.998	2.72	43.54	0.0200	0.0278
0.3000	18.000	2.72	43.54	0.0200	0.0278
0.3166	18.996	2.72	43.54	0.0200	0.0278
0.3333	19.998	2.73	43.55	0.0100	0.0139
0.4167	25.002	2.73	43.55	0.0100	0.0139
0.5000	30.000	2.73	43.55	0.0100	0.0139
0.5833	34.998	2.73	43.55	0.0100	0.0139
0.6667	40.002	2.73	43.55	0.0100	0.0139
0.7500	45.000	2.73	43.55	0.0100	0.0139
0.8333	49.998	2.73	43.55	0.0100	0.0139
0.9167	55.002	2.73	43.55	0.0100	0.0139
1.0000	60.000	2.73	43.55	0.0100	0.0139
1.0833	64.998	2.73	43.55	0.0100	0.0139
1.1667	70.002	2.73	43.55	0.0100	0.0139
1.2500	75.000	2.73	43.55	0.0100	0.0139
1.3330	79.980	2.73	43.55	0.0100	0.0139
1.4166 -	84.996	2.73	43.55	0.0100	0.0139
1.5000	90.000	2.73	43.55	0.0100	0.0139
1.5800	94.800	2.73	43.55	0.0100	0.0139
1.6667	100.002	2.73	43.55	0.0100	0.0139
1.7500	105.002	2.73	43.55	0.0100	0.0139
1.8333	109.998	2.73	43.55	0.0100	0.0139
1.9167	115.002	2.73	43.55	0.0100	0.0139
2.0000	120.000	2.73	43.55	0.0100	0.0139
2.000	120.000	4.13	45.55	0.0100	0.0172

#### SLUG TEST DATA - WELL MW-5D Performed November 21, 1994

Time (min)	Time (sec)	Value (feet)	Elevation (feet)	Change (h)	Head Ratio (h/h <sub>0</sub> )
0.0833	4.998	6.41	42.49	0.7300	1.0000
0.1000	6.000	6.41	42.49	0.7300	1.0000
0.1166	6.996	6.43	42.51	0.7100	0.9726
0.1333	7.998	6.44	42.52	0.7000	0.9589
0.1500	9.000	6.44	42.52	0.7000	0.9589
0.1666	9.996	6.45	42.53	0.6900	0.9452
0.1833	10.998	6.46	42.54	0.6800	0.9315
0.2000	12.000	6.46	42.54	0.6800	0.9315
0.2166	12.996	6.46	42.54	0.6800	0.9315
0.2333	13.998	6.47	42.55	0.6700	0.9178
0.2500	15.000	6.48	42.56	0.6600	0.9041
0.2666	15.996	6.48	42.56	0.6600	0.9041
0.2833	16.998	6.48	42.56	0.6600	0.9041
0.3000	18.000	6.49	42.57	0.6500	0.8904
0.3166	18.996	6.49	42.57	0.6500	0.8904
0.3333	19.998	6.50	42.58	0.6400	0.8767
0.4167	25.002	6.52	42.60	0.6200	0.8493
0.5000	30.000	6.54	42.62	0.6000	0.8219
0.5833	34.998	6.56	42.64	0.5800	0.7945
0.6667	40.002	6.57	42.65	0.5700	0.7808
0.7500	45.000	6.58	42.66	0.5600	0.7671
0.8333	49.998	6.60	42.68	0.5400	0.7397
0.9167	55.002	6.61	42.69	0.5300	0.7260
1.0000	60.000	6.63	42.71	0.5100	0.6986
1.0833	64.998	6.64	42.72	0.5000	0.6849
1.1667	70.002	6.65	42.73	0.4900	0.6712
1.2500	75.000	6.66	42.74	0.4800	0.6575
1.3330	79.980	6.67	42.75	0.4700	0.6438
1.4166	84.996	6.69	42.77	0.4500	0.6164
1.5000	90.000	6.70	42.78	0.4400	0.6027
1.5800	94.800	6.71	42.79	0.4300	0.5890
1.6667	100.002	6.72	42.80	0.4200	0.5753
1.7500	105.000	6.73	42.81	0.4100	0.5616
1.8333	109.998	6.74	42.82	0.4000	0.5479
1.9167	115.002	6.75	42.83	0.3900	0.5342
2.0000	120.000	6.76	42.84	0.3800	0.5205
2.5000	150.000	6.81	42.89	0.3300	0.4521
3.0000	180.000	6.85	42.93	0.2900	0.3973
3.5000	210.000	6.89	42.97	0.2500	0.3425
4.0000	240.000	6.92	43.00	0.2200	0.3014
4.5000	270.000	6.95	43.03	0.1900	0.2603
5.0000	300.000	6.97	43.05	0.1700	0.2329
5.5000	330.000	6.99	43.07	0.1500	0.2055
6.0000	360.000	7.00	43.08	0.1400	0.1918
6.5000	390.000	7.02	43.10	0.1200	0.1644
7.0000	420.000	7.03	43.11	0.1100	0.1507
7.5000	450.000	7.04	43.12	0.1000	0.1370
8.0000	480.000	7.05	43.13	0.0900	0.1233
8.5000	510.000	7.06	43.14	0.0800	0.1096
9.0000	540.000	7.07	43.15	0.0700	0.0959
9.5000	570.000	7.08	43.16	0.0600	0.0822

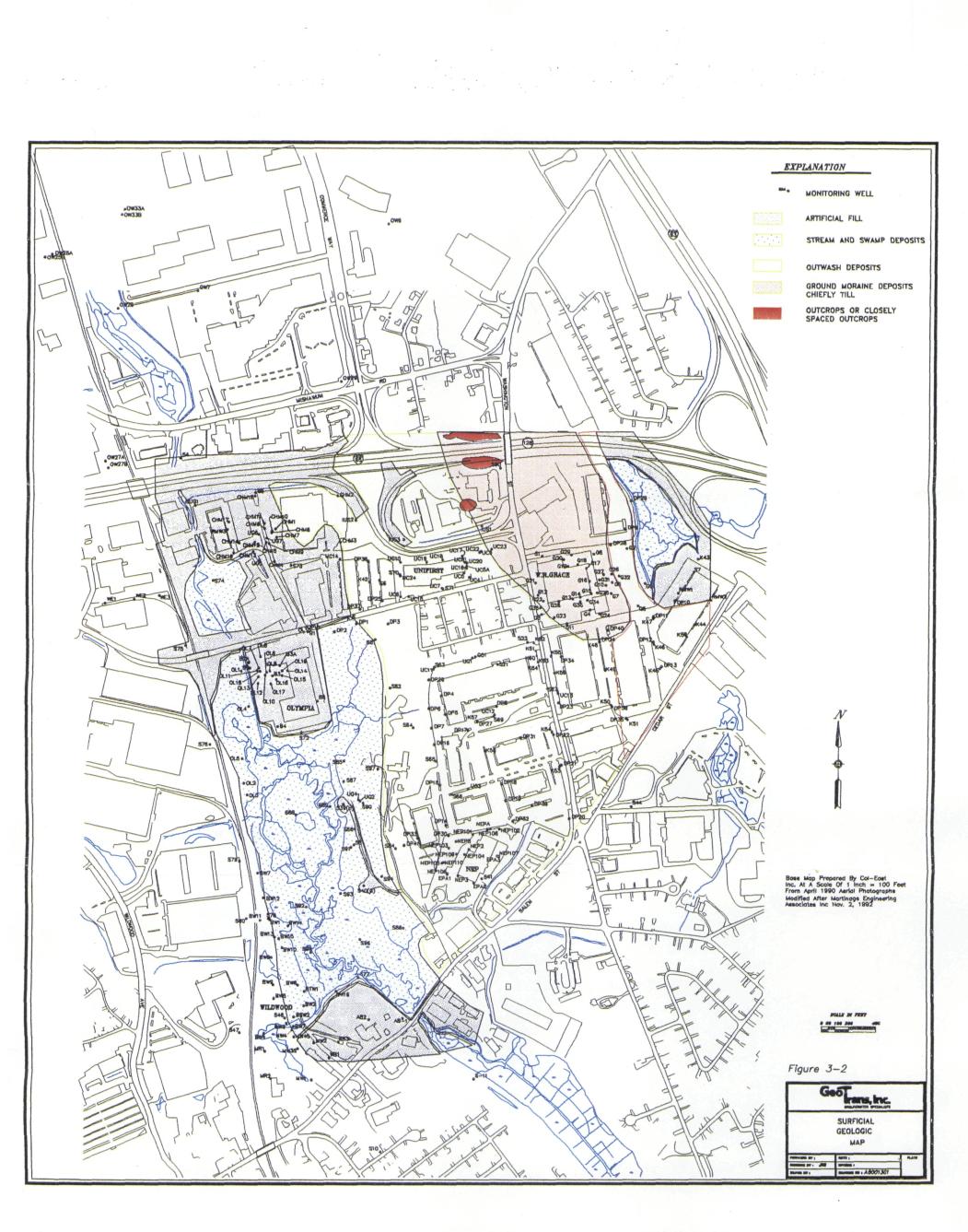
#### SLUG TEST DATA - WELL MR-1SS Performed November 21, 1994

Time (min)	Time	Value	Elevation	Change (h)	Head Ratio (h/h <sub>0</sub> )
(111111)	(sec)	(feet)	(feet)	(11)	/ivii07
0.0666	3.996	2.63	41.52	0.4100	1.0000
0.0833	4.998	2.76	41.65	0.2800	0.6829
0.1000	6.000	2.70	41.73	0.2000	0.4878
0.1500	9.000	2.86	41.75	0.1800	0.4390
0.1666	9.996	2.89	41.78	0.1500	0.3659
0.1833	10.998	2.91	41.80	0.1300	0.3035
0.2000	12.000	2.91	41.80	0.1300	0.3171
0.2166	12.996	2.92	41.81	0.1200	0.2927
0.2333	13.998	2.92	41.81	0.1200	0.2927
0.2500	15.000	2.93	41.82	0.1200	0.2683
0.2666	15.996	2.93	41.82	0.1100	0.2683
0.2833	16.998	2.93	41.82	0.1100	0.2683
0.3000	18.000	2.94	41.83	0.1100	0.2439
0.3166	18.996	2.94	41.83	0.1000	0.2439
0.3333	19.998	2.95	41.84	0.1000	0.2195
0.4167	25.002	2.97	41.86	0.0700	0.1707
0.5000	30.000	2.98	41.87	0.0600	0.1463
0.5833	34.998	2.99	41.88	0.0500	0.1403
0.6667	40.002	3.00	41.89	0.0400	0.0976
0.7500	45.000	3.01	41.90	0.0300	0.0773
0.8333	49.998	3.01	41.90	0.0300	0.0732
0.9167	55.002	3.02	41.91	0.0200	0.0488
1.0000	60.000	3.02	41.91	0.0200	0.0488
1.0833	64.998	3.02	41.91	0.0200	0.0488
1.1667	70.002	3.02	41.91	0.0200	0.0488
1.2500	75.000	3.02	41.91	0.0200	0.0488
1.3330	79.980	3.02	41.91	0.0200	0.0488
1.4166	84.996	3.03	41.92	0.0100	0.0244
1.5000	90.000	3.03	41.92	0.0100	0.0244
1.5800	94.800	3.03	41.92	0.0100	0.0244
1.6667	100.002	3.03	41.92	0.0100	0.0244
1.7500	105.000	3.03	41.92	0.0100	0.0244
1.8333	109.998	3.03	41.92	0.0100	0.0244
1.9167	115.002	3.03	41.92	0.0100	0.0244
2.0000	120.000	3.03	41.92	0.0100	0.0244

## SLUG TEST DATA - WELL MR-2SS Performed November 21, 1994

Time	Time	Value	Elevation	Change	Head Ratio
<u>(min)</u>	(sec)	(feet)	(feet)	(h)	(h/h <sub>o</sub> )
0.0000	0.504	2.45	40.00	0.0400	1 0000
0.0099	0.594	2.47	43.22	0.3400	1.0000
0.0133	0.798	2.56	43.31	0.2500	0.7353
0.0266	1.596	2.60	43.35	0.2100	0.6177
0.0666	3.996	2.63	43.38	0.1800	0.5294
0.0833	4.998	2.70	43.45	0.1100	0.3235
0.1000	6.000	2.73	43.48	0.0800	0.2353
0.1166	6.996	2.74	43.49	0.0700	0.2059
0.1333	7.998	2.75	43.50	0.0600	0.1765
0.1500	9.000	2.75	43.50	0.0600	0.1765
0.1666	9.996	2.76	43.51	0.0500	0.1471
0.1833	10.998	2.76	43.51	0.0500	0.1471
0.2000	12.000	2.76	43.51	0.0500	0.1471
0.2166	12.996	2.77	43.52	0.0400	0.1176
0.2333	13.998	2.77	43.52	0.0400	0.1176
0.2500	15.000	2.77	43.52	0.0400	0.1176
0.2666	15.996	2.77	43.52	0.0400	0.1176
0.2833	16.998	2.77	43.52	0.0400	0.1176
0.3000	18.000	2.78	43.53	0.0300	0.0882
0.3166	18.996	2.78	43.53	0.0300	0.0882
0.3333	19.998	2.78	43.53	0.0300	0.0882
0.4167	25.002	2.78	43.53	0.0300	0.0882
0.5000	30.000	2.79	43.54	0.0200	0.0588
0.5833	34.998	2.79	43.54	0.0200	0.0588
0.6667	40.002	2.79	43.54	0.0200	0.0588
0.7500	45.000	2.79	43.54	0.0200	0.0588
0.8333	49.998	2.79	43.54	0.0200	0.0588
0.9167	55.002	2.79	43.54	0.0200	0.0588
1.0000	60.000	2.79	43.54	0.0200	0.0588
1.0833	64.998	2.79	43.54	0.0200	0.0588
1.1667	70.002	2.79	43.54	0.0200	0.0588
1.2500	75.000	2.79	43.54	0.0200	0.0588
1.3330	79.980	2.79	43.54	0.0200	0.0588
1.4166	84.996	2.79	43.54	0.0200	0.0588
1.5000	90.000	2.79	43.54	0.0200	0.0588
1.5800	94.800	2.79	43.54	0.0200	0.0588
1.6667	100.002	2.79	43.54	0.0200	0.0588
1.7500	105.000	2.80	43.55	0.0100	0.0294
1.8333	109.998	2.80	43.55	0.0100	0.0294
1.9167	115.002	2.80	43.55	0.0100	0.0294
2.0000	120.000	2.80	43.55	0.0100	0.0294

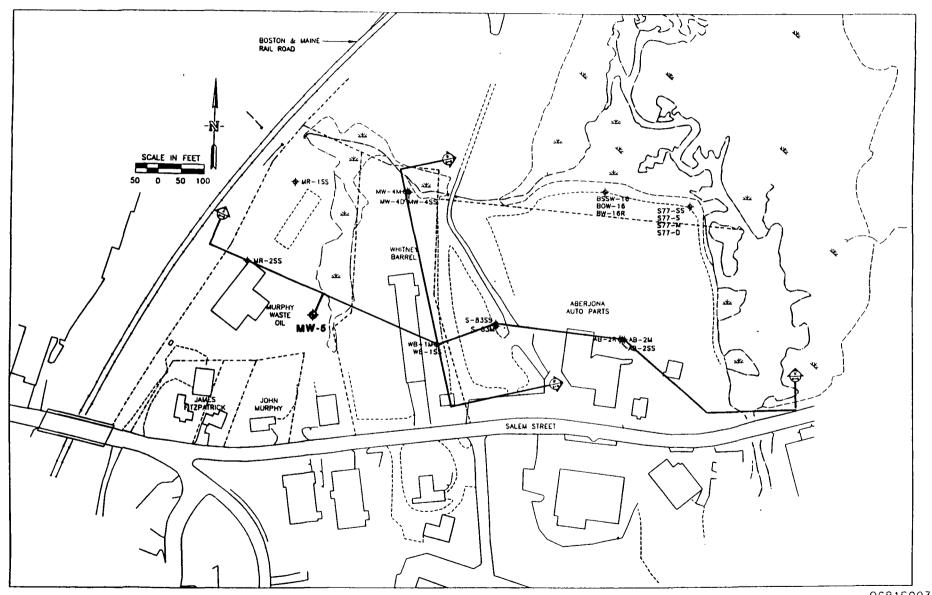
# APP T



#### NOTE:

MODIFIED TO SHOW MONITORING WELL MW-5 WHICH WAS INSTALLED BY CLEAN HARBORS ENVIRONMENTAL SERVICES, INC. ON OCTOBER 14 THROUGH 18, 1994.

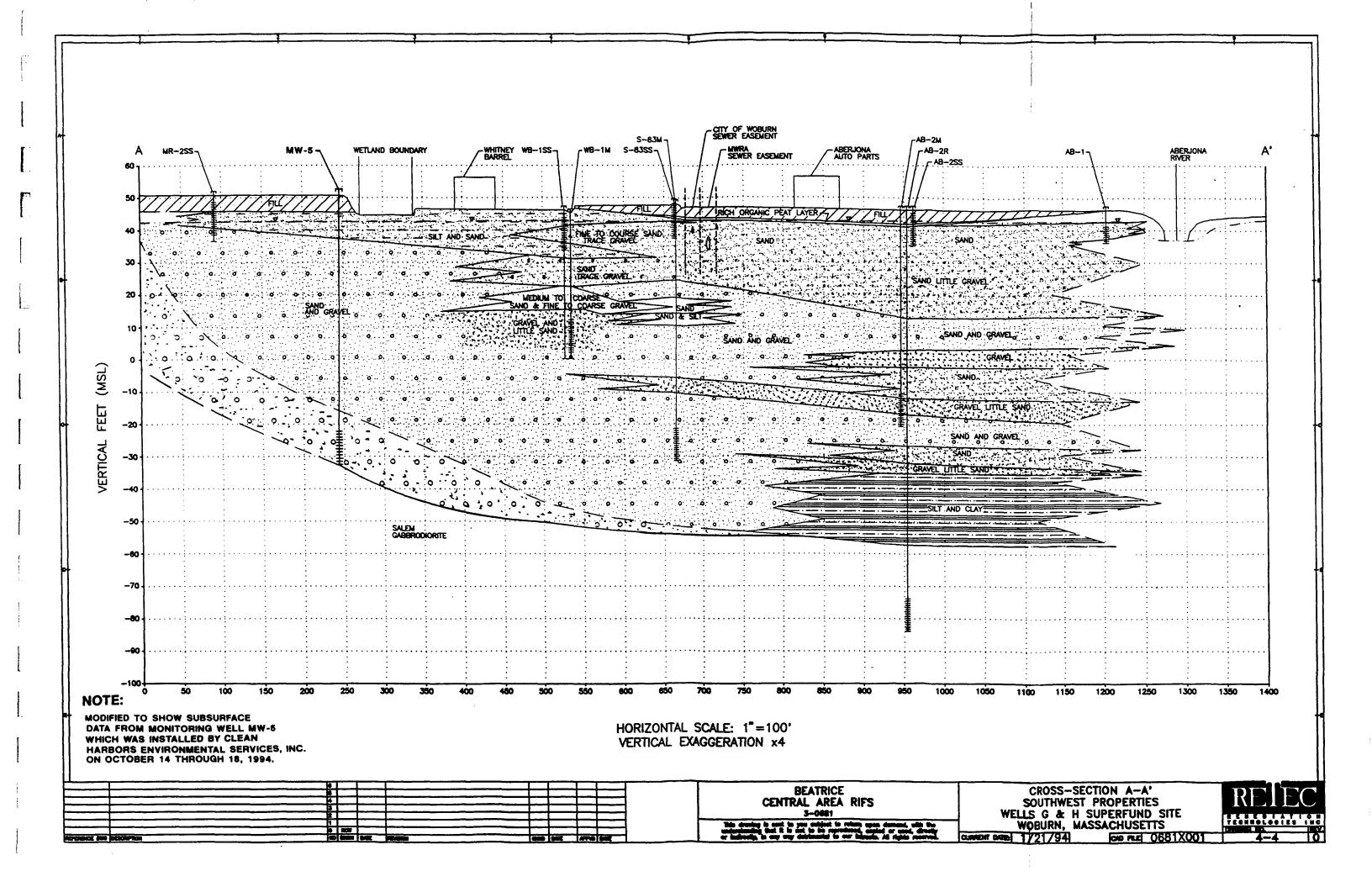


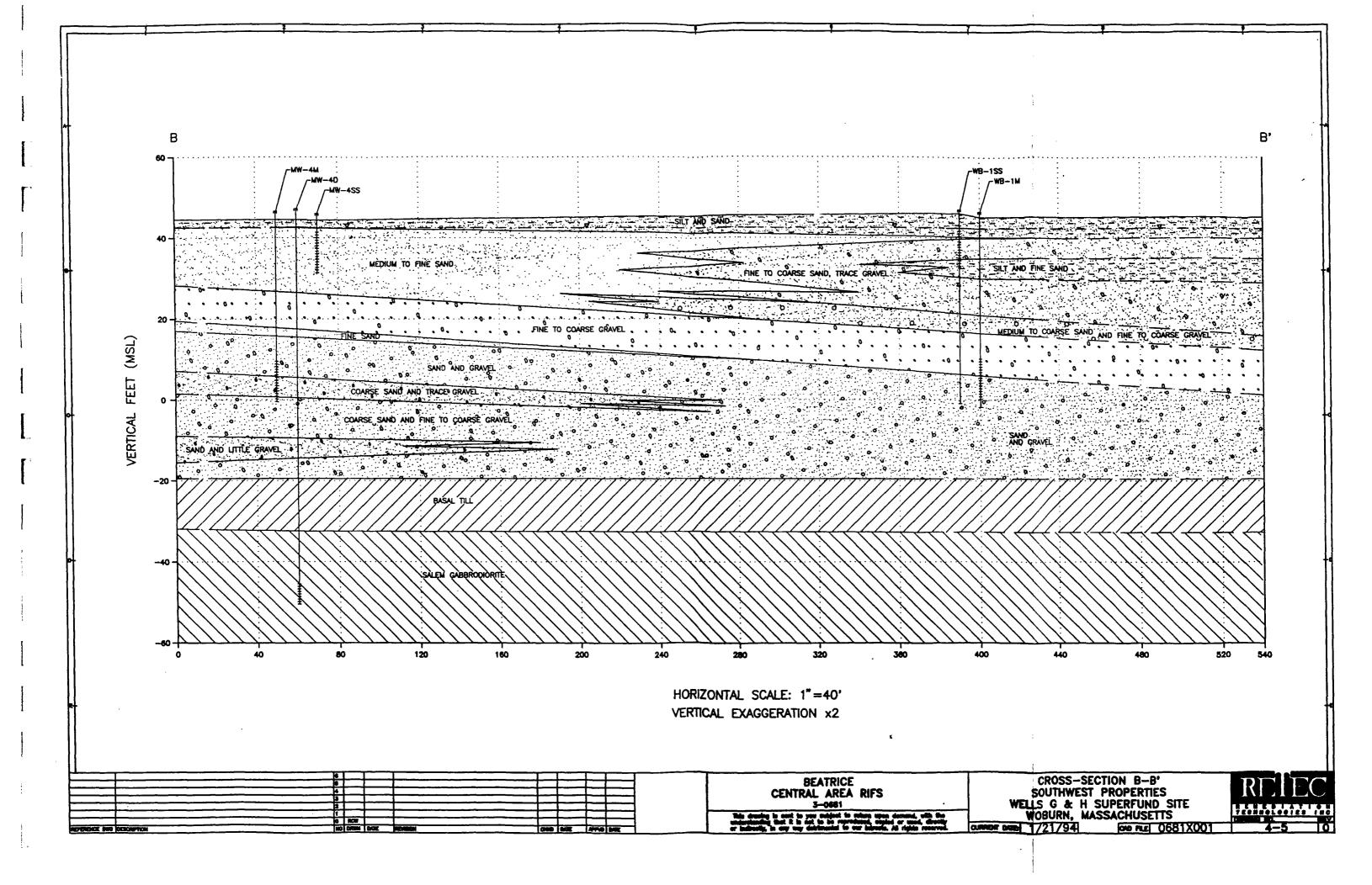


**CROSS-SECTION LOCATIONS** 

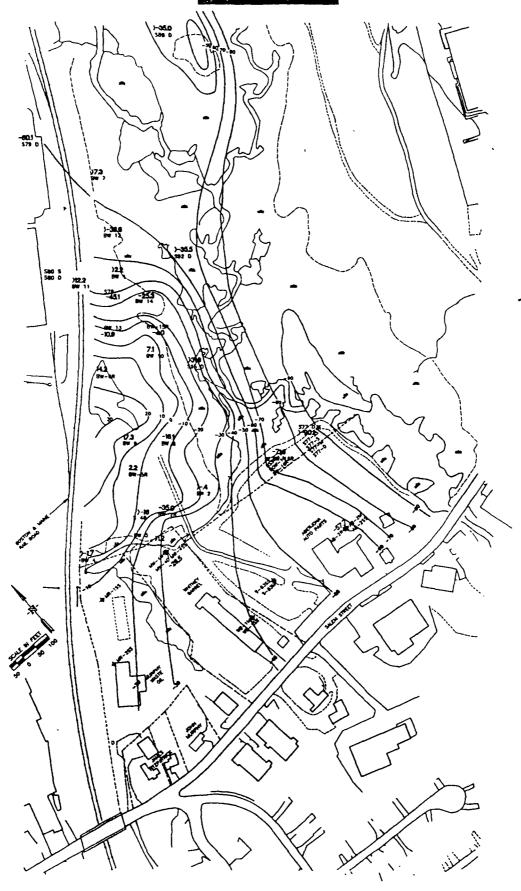
06815003

FIGURE

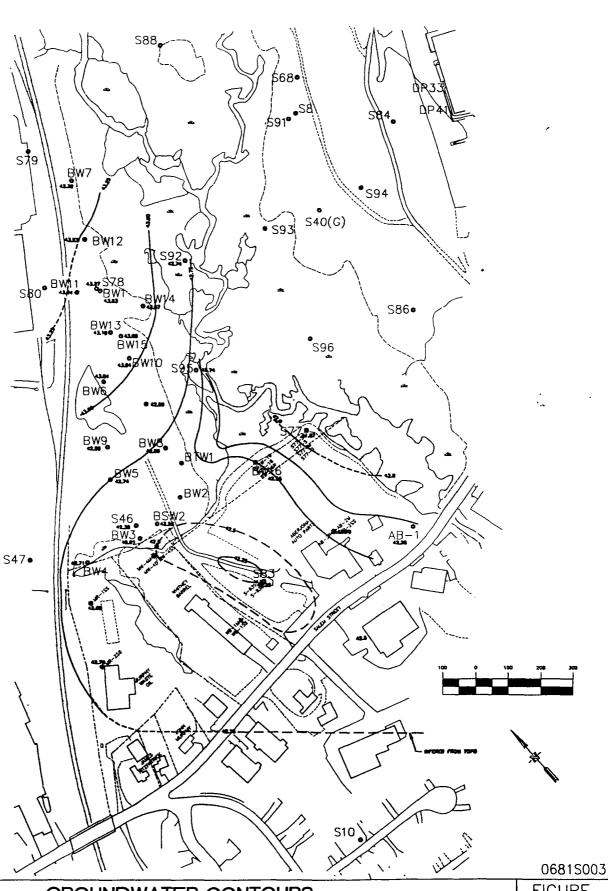








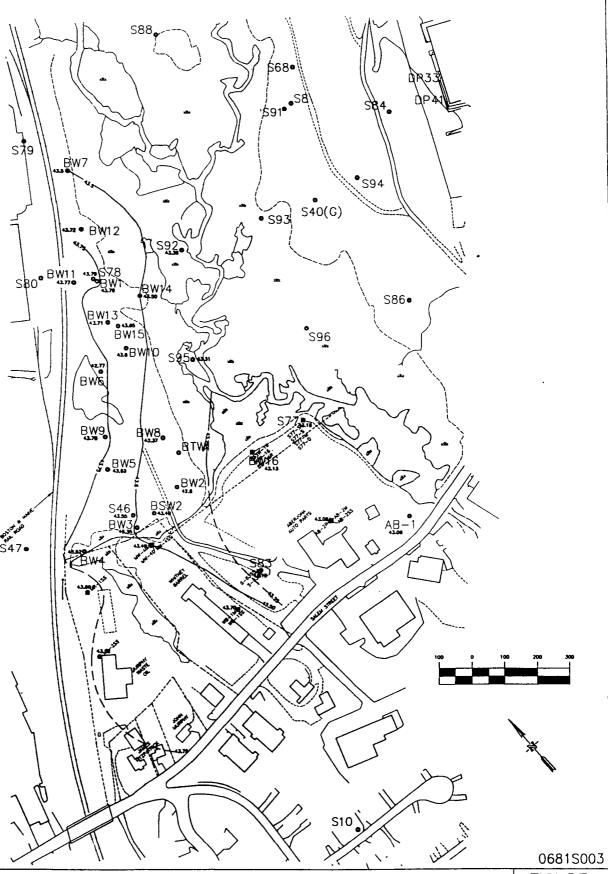
0681S003 FIGURE



**GROUNDWATER CONTOURS** SEPTEMBER 7, 1993

FIGURE

#### RELEC



GROUNDWATER CONTOURS NOVEMBER 30, 1993 FIGURE